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台灣計算力學學會
專題演講 暨 會員交流活動

NTU, Taipei | March 28, 2023



Continuum Mechanics of Extreme Response Analysis and
Measurement Noise Reduction for Stokes flow under Uncertainty

考慮不確定性於斯托克斯流場域
極值反應解析與量測數據降噪之連體力學研究

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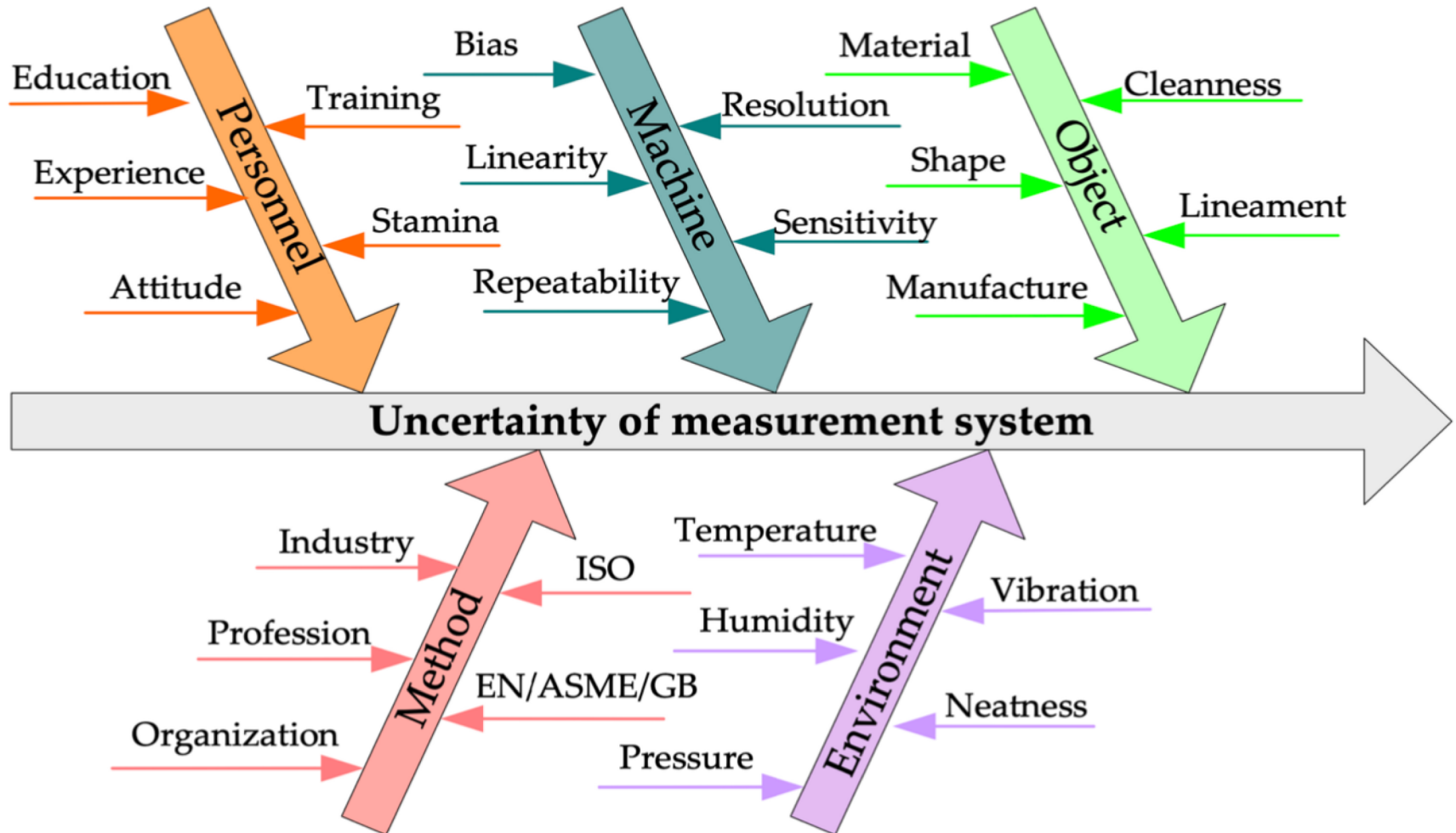
Measurement Noise Reduction

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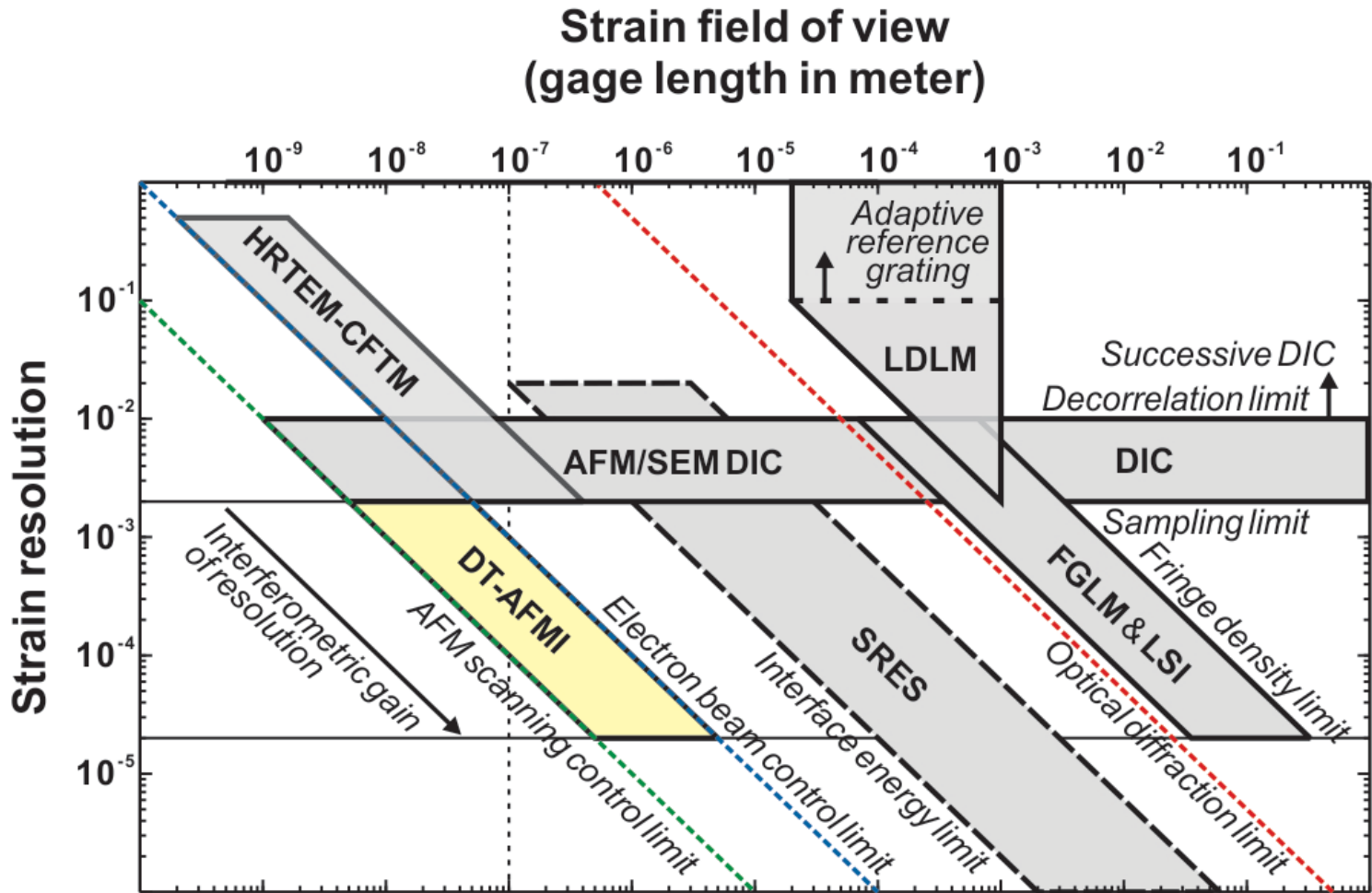
Conclusion



Introduction – Uncertainty of measurement system



Deformation measurement map

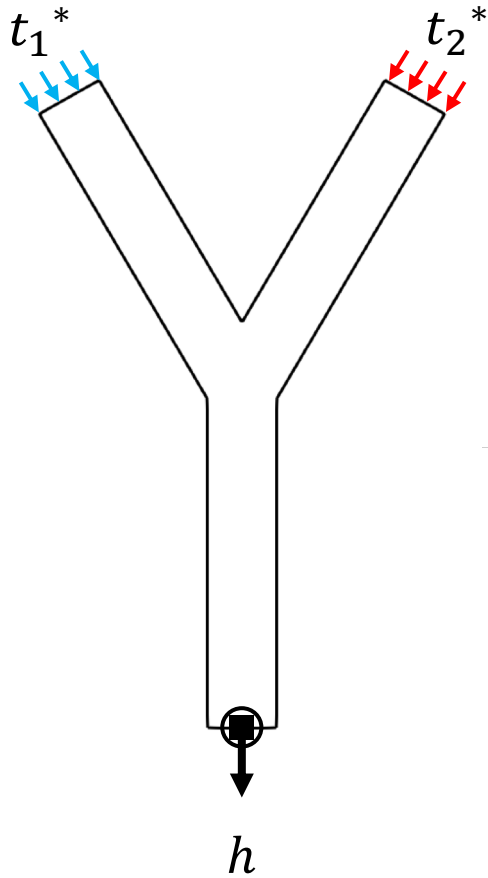


- ▶ **Strain resolution** of measurements can be effectively **gained** from **interferometry** techniques.
- ▶ **Interferometry** utilizes **precise lattice grating** for deformation measurement with high strain resolution in **small observation windows**.

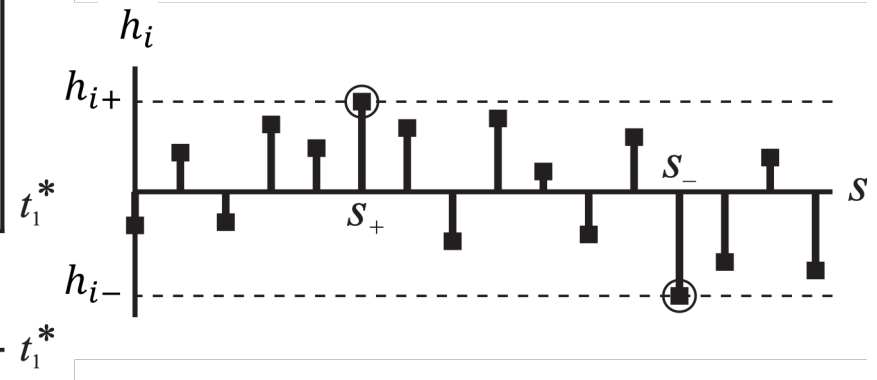
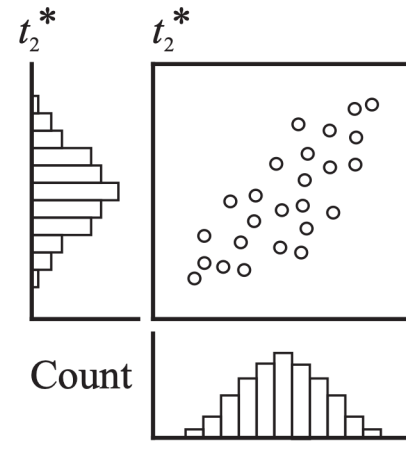
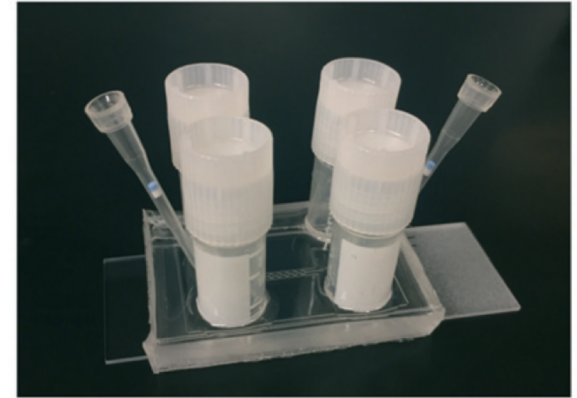


Motivation – Extreme response analysis for Stokes flow

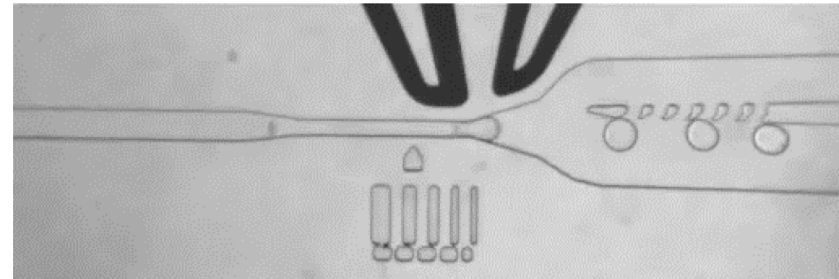
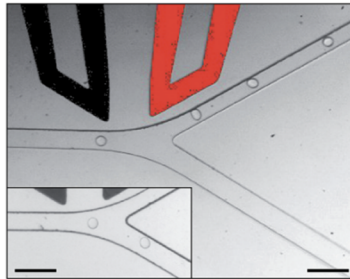
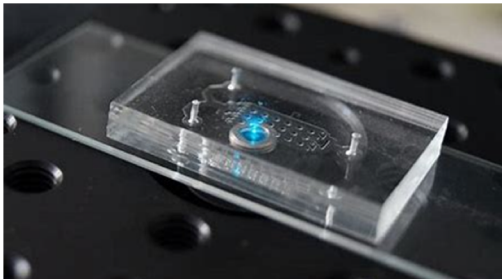
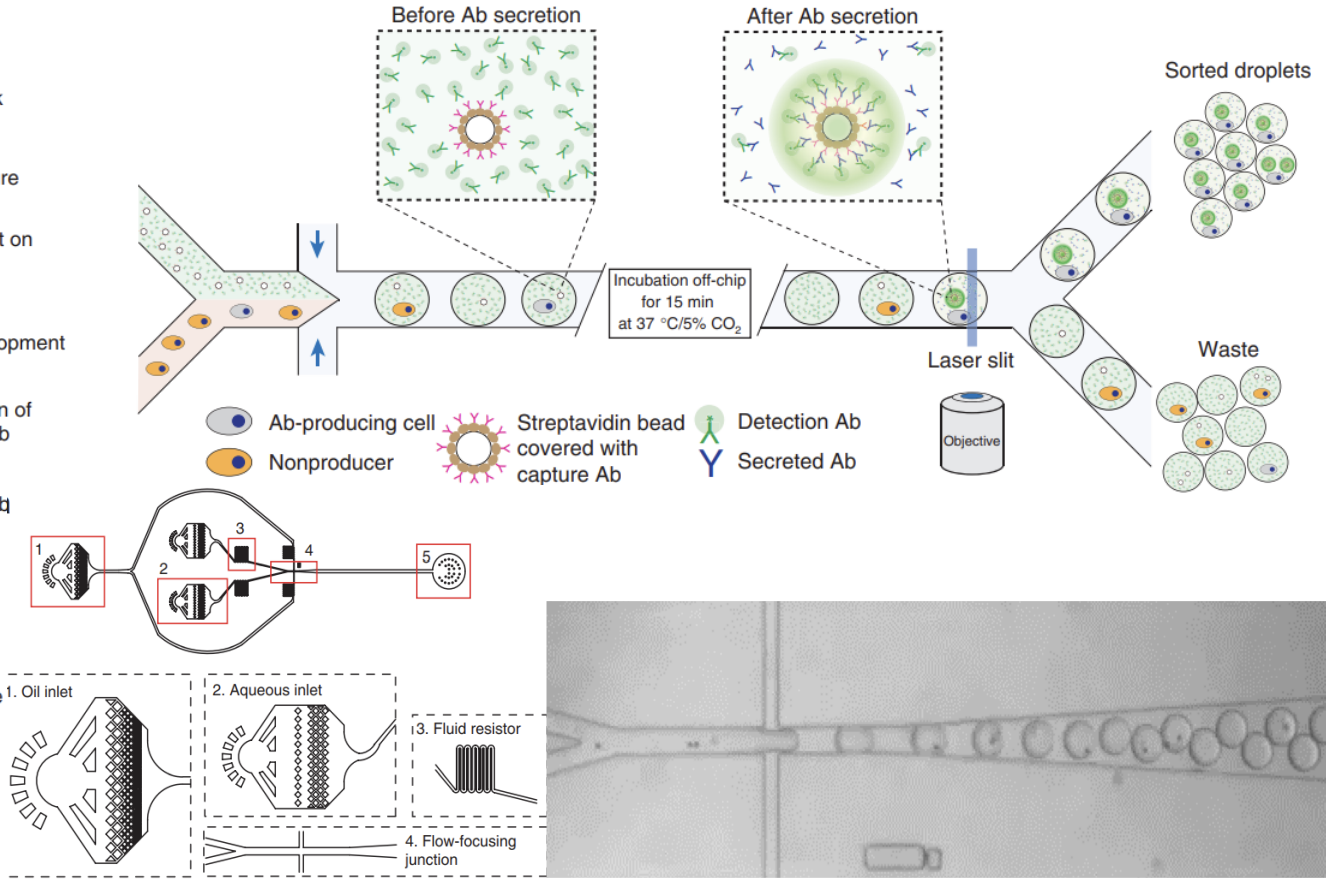
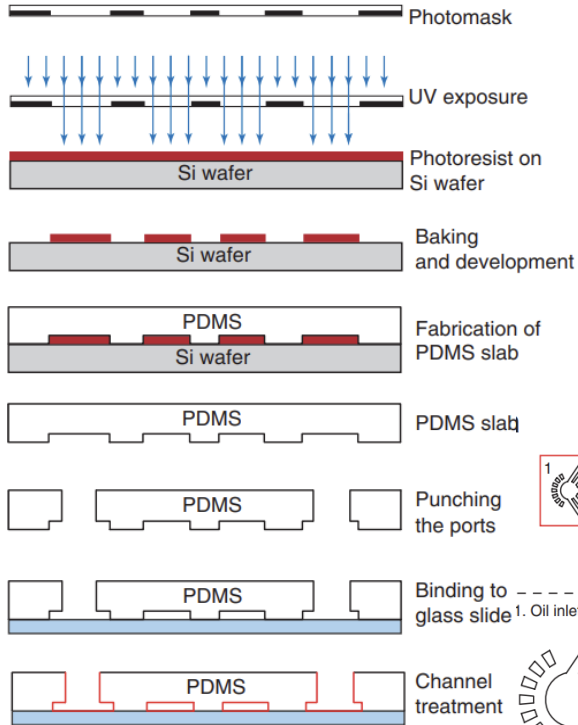
Microfluidic system



Uncertainty



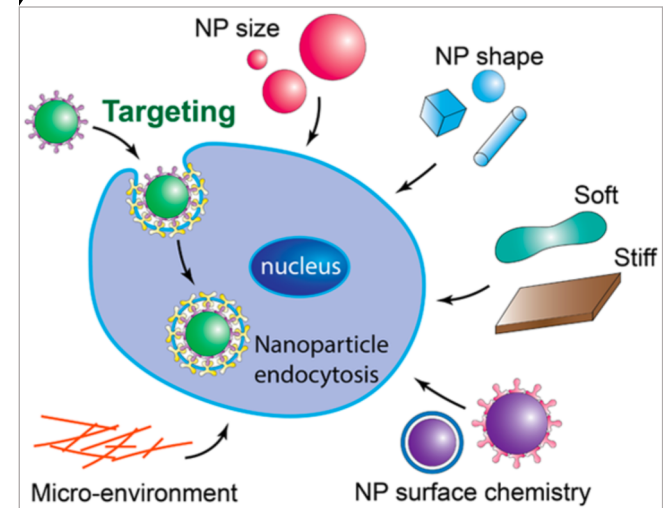
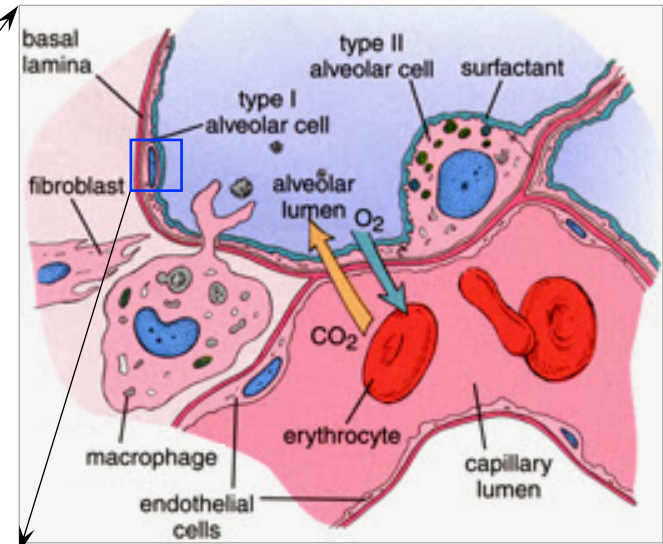
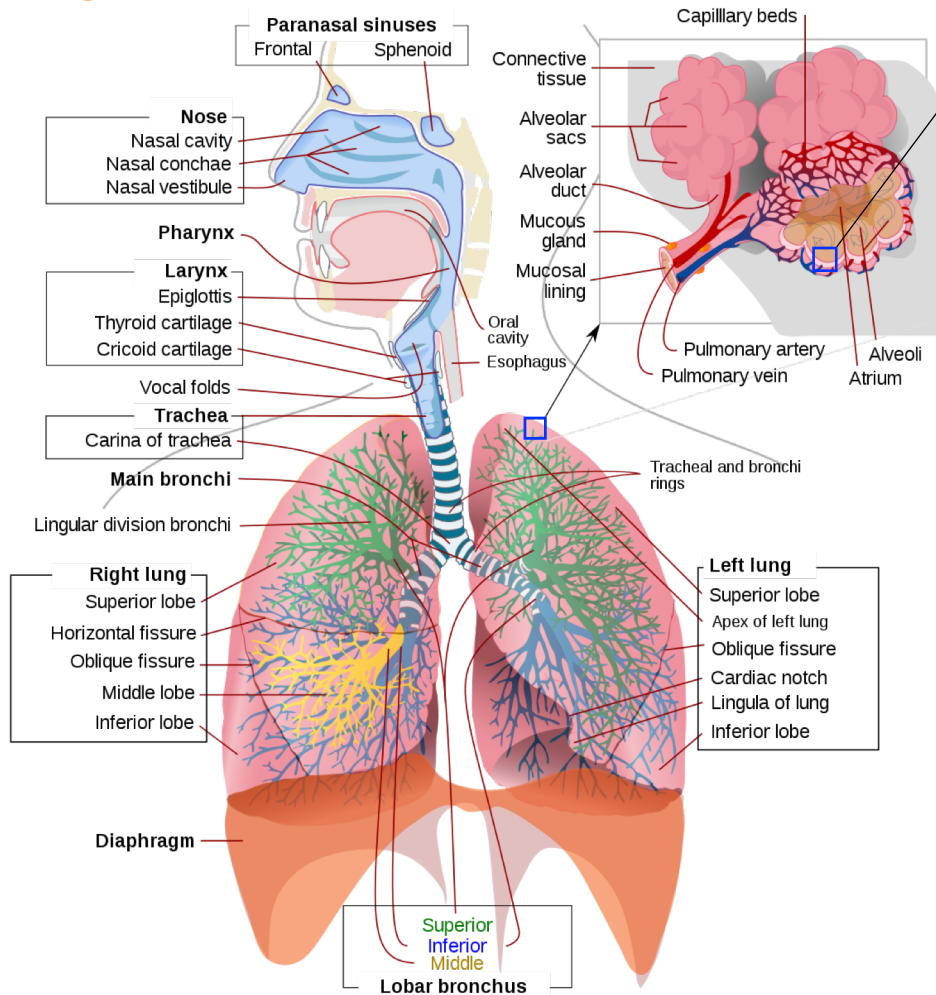
Fluorescence-activated droplet sorting experiment





Measurement of oxygen diffusivity of live cell layers

Biological and environmental interactions

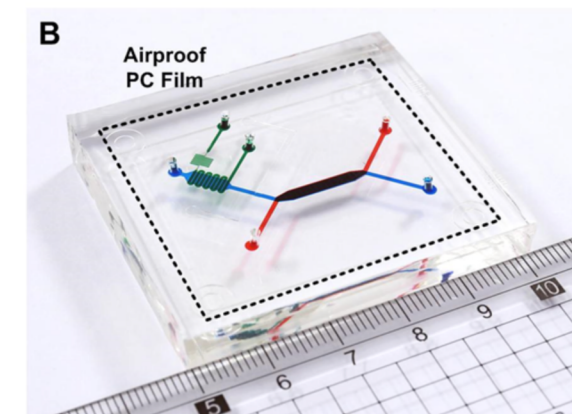
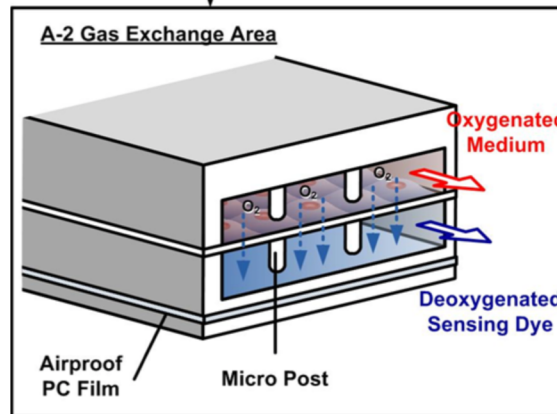
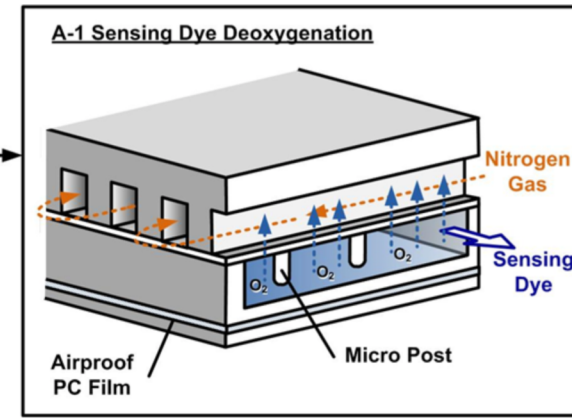
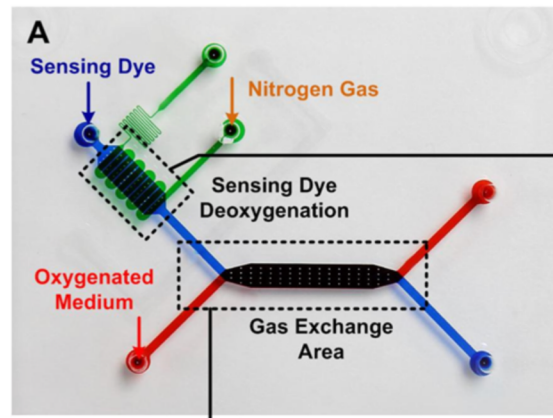
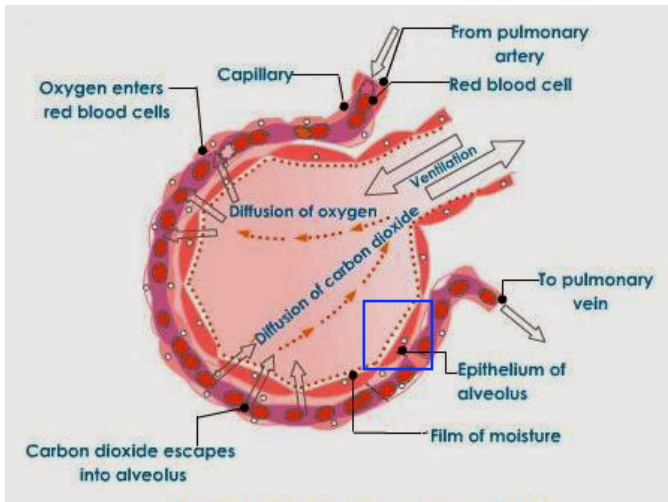


- ▶ Different studies have been reported to examine experimental **oxygen diffusivity** for simple **membrane** or **single-celled organisms**.
- ▶ However, proper investigation on **oxygen transportation through cell layers** have not been done.



Measurement of oxygen diffusivity of live cell layers

Biological and environmental interactions



(1) Fick's first law of diffusion

$$J = D \left[\frac{C_A - C(x)}{d} \right]$$

(2) Mass conservation

$$\frac{dC(x)}{dx} + \frac{D}{dhv} [C(x) - C_A] = 0$$

(3) Oxygen tension profile

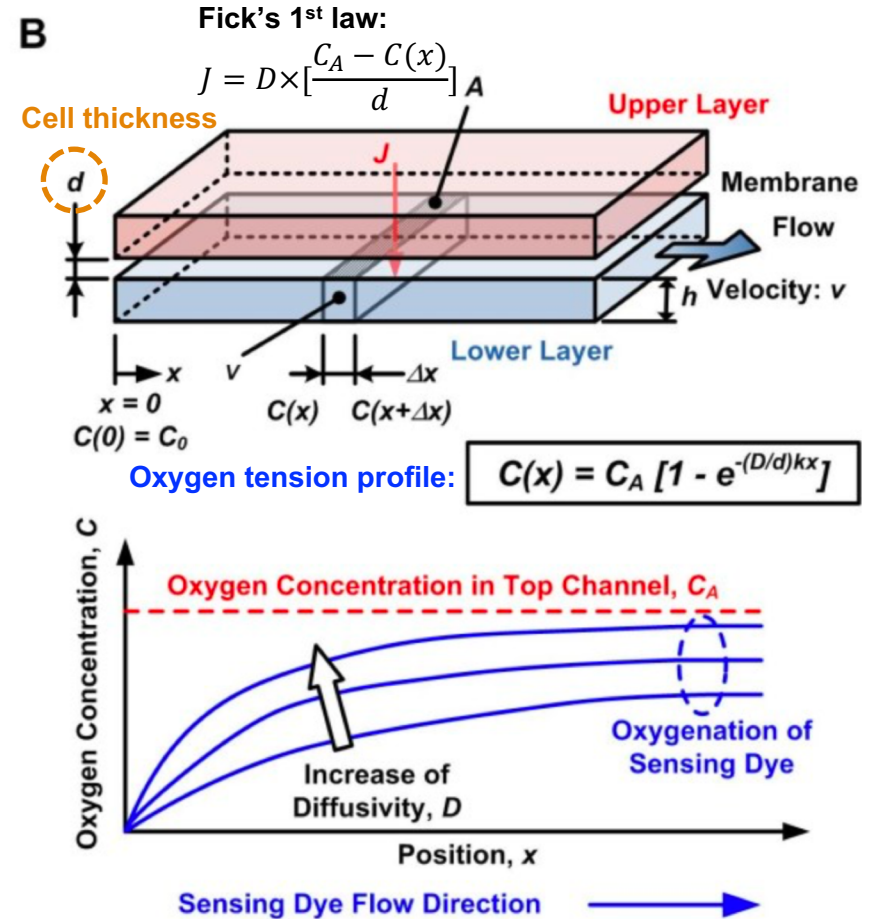
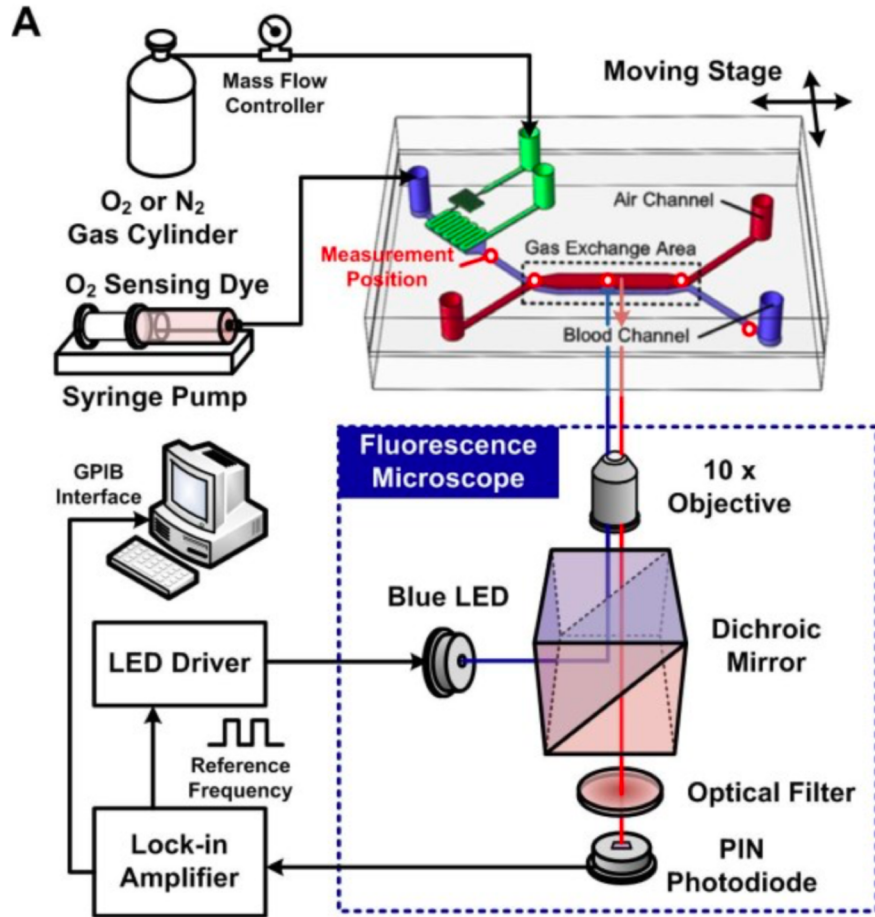
$$C(x) = C_A \times \left[1 - e^{-\left(\frac{D}{dhv}\right)x} \right]$$

- ▶ Effects of environmental matter states (solid, liquid, gas, plasma) on **cell uptake**
- ▶ Cell entry pathways of **gas diffusion**
- ▶ Some particular cells might **accelerate oxygen transportation**

Measurement of oxygen diffusivity of live cell layers



Biological and environmental interactions



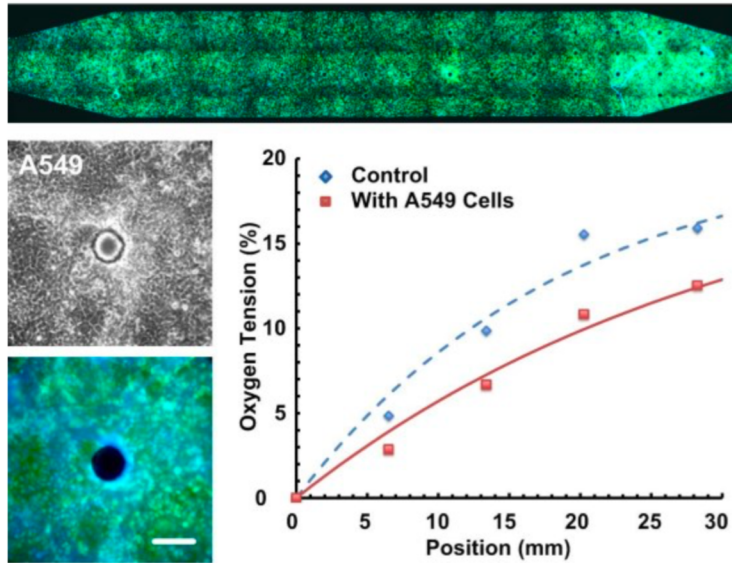
- ▶ **Lifetime fluorescence** measurement system for probing **oxygen tensions** in **microfluidic channel**
- ▶ **Fluidic actuation** achieved by a **computer-controlled syringe pump**
- ▶ **Theoretical model** for estimating **oxygen tension profile** in the bottom microfluidic channel with the **membrane of different oxygen diffusivity**

Measurement of oxygen diffusivity of live cell layers

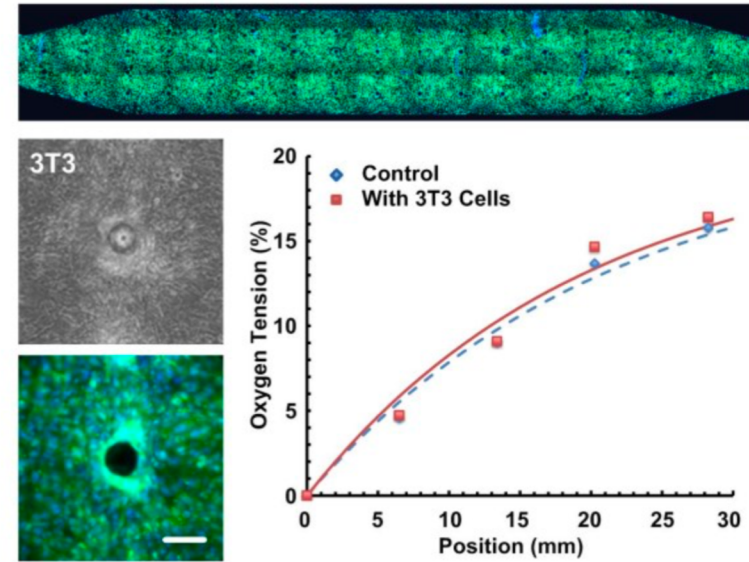


Biological and environmental interactions

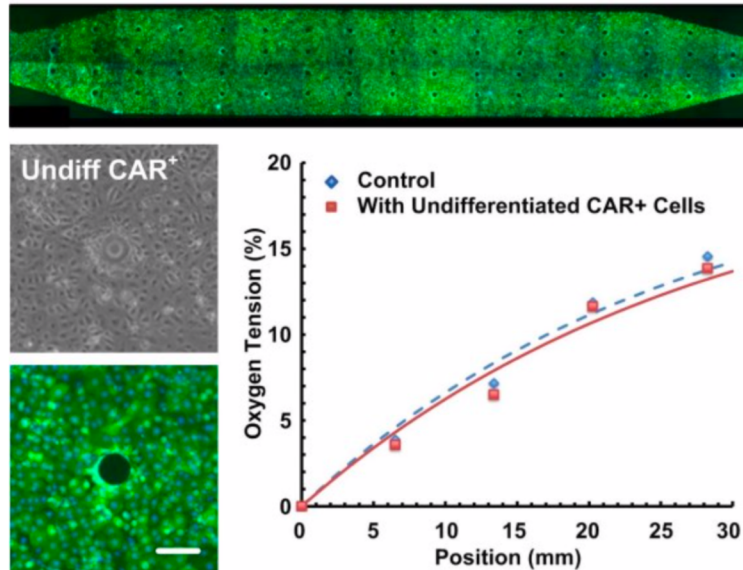
A A549 Cells (Calcein AM/Hoechst)



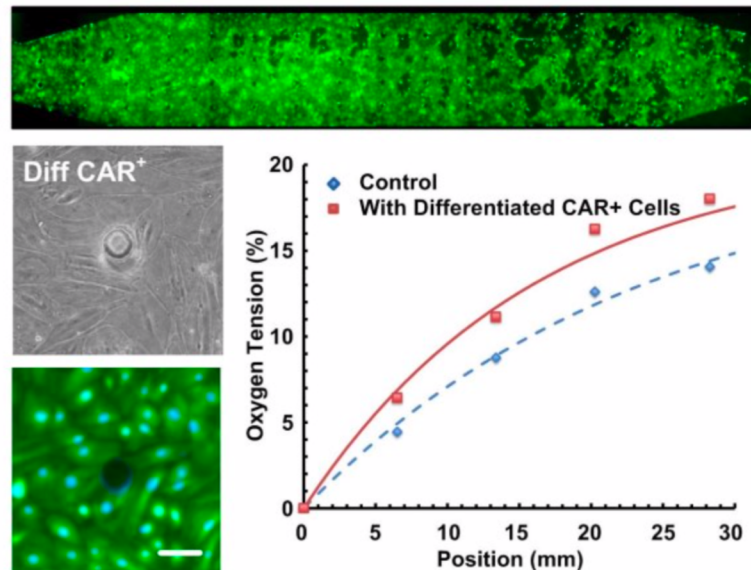
B 3T3 Cells (Calcein AM/Hoechst)



A Undifferentiated CAR⁺ Cells (Calcein AM/Hoechst)



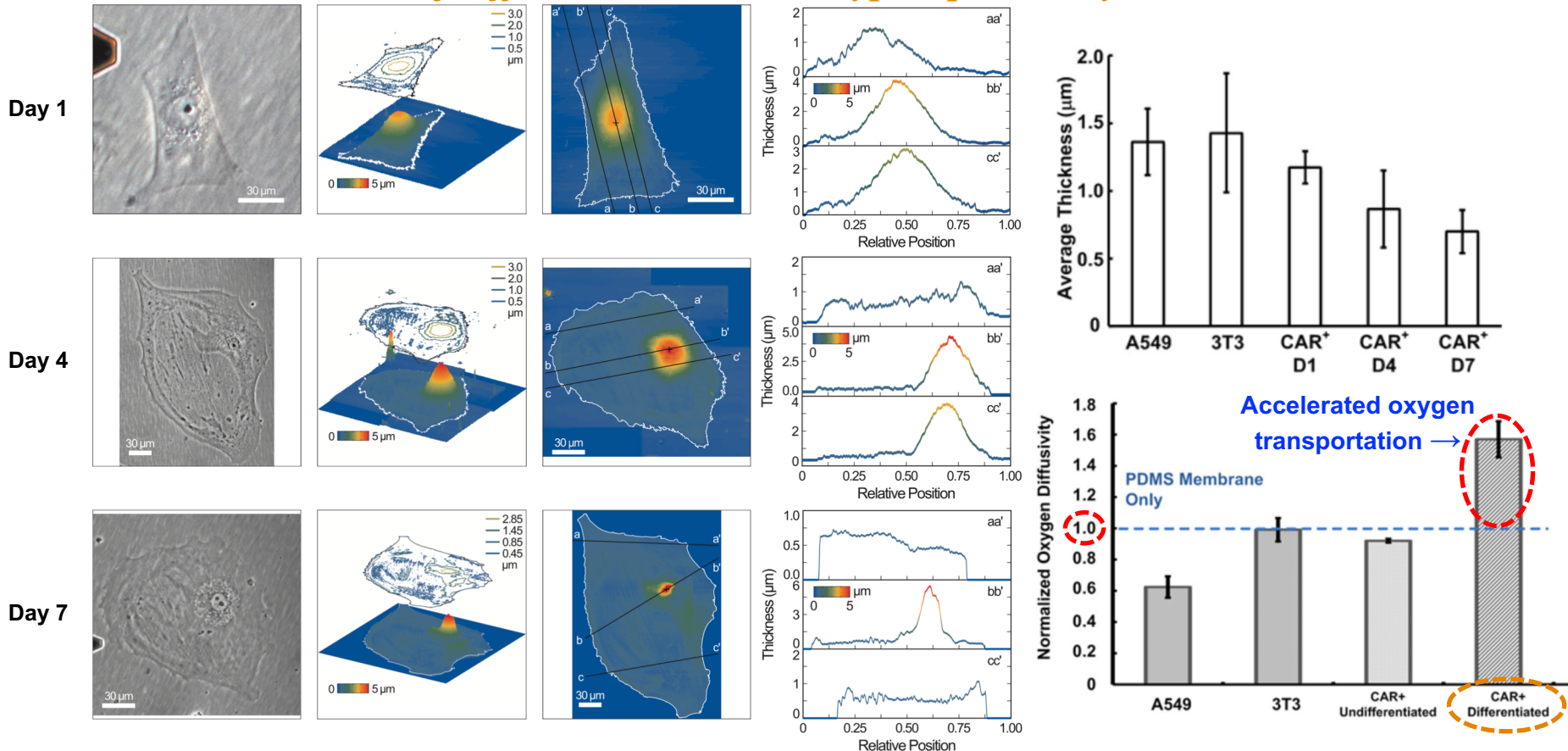
B Differentiated CAR⁺ Cells (T1 α /Hoechst)



Bio-AFM & oxygen diffusivity of live cell layers



Bio-AFM measurement of differentiated alveolar type-I pneumocytes-like (dAT-I-like)/cells

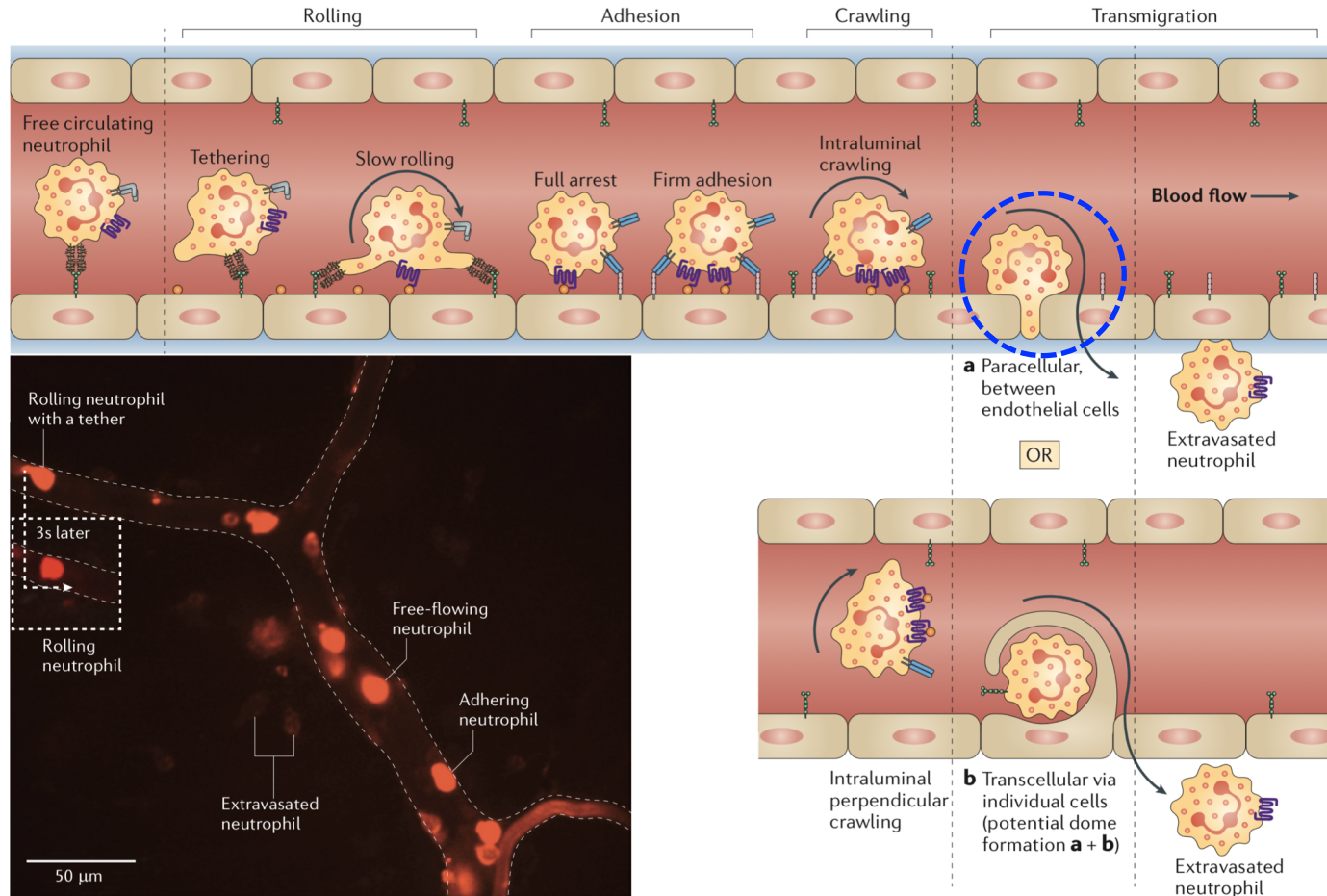


- ▶ Distinct **facilitated oxygen diffusion** behavior of the dAT-I-like/cells
- ▶ Comparison with A549 cells (human adenocarcinoma originated from alveolar type-II pneumocyte) and 3T3 cells (murine fibroblast)
- ▶ **Drug testing** to seek possible therapeutic strategies to **improve oxygenation** in patients with **pulmonary dysfunction**, such as premature infants with bronchopulmonary dysplasia & adults with chronic obstructive pulmonary disease (COPD)



Measurement of in-plane elasticity of live cell layers

Neutrophil recruitment cascade & extravasation

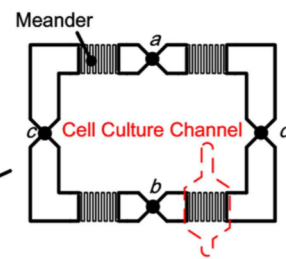
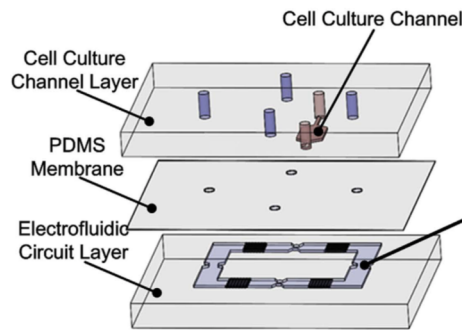
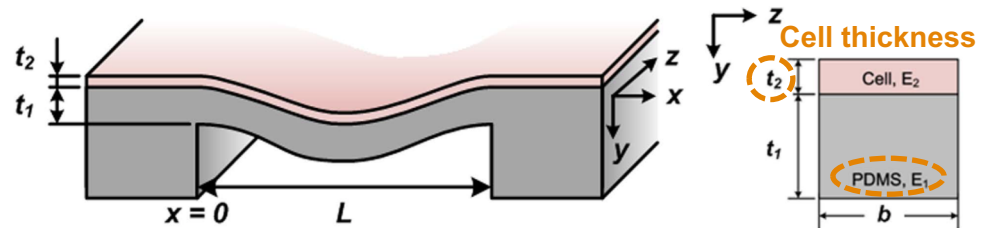
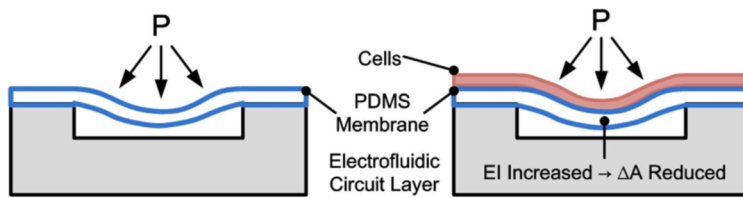


- ▶ **Endothelial membrane:** A continuous structure having ECM proteins - collagens & laminins
- ▶ **Neutrophils:** Releasing neutrophil elastase against ECM protein to pass through the membrane
- ▶ **Endothelium in-plane elasticity:** Having effects on the interaction between vessel wall surfaces and bloodstream carrying white and red blood cells in hemodynamic systems

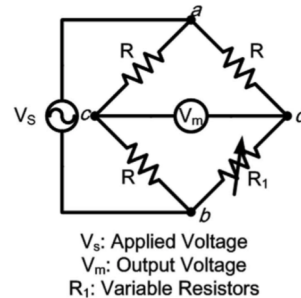
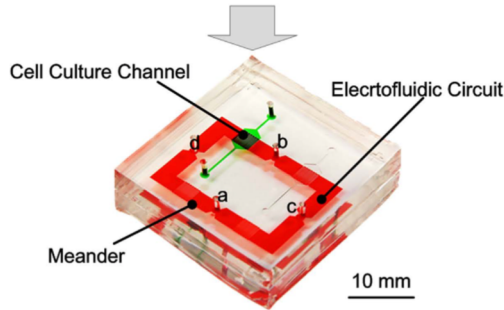


Measurement of in-plane elasticity of live cell layers

Microfluidic device development & mechanical model derivation



a, b: Signal Input (Applied Voltage)
c, d: Signal Output (Output Voltage)



(1) Euler–Bernoulli beam theory

$$u_y(x) = \frac{P}{EI} \left(\frac{x^4}{24} - \frac{Lx^3}{12} + \frac{L^2x^2}{24} \right)$$

(2) Kirchhoff's law on a Wheatstone bridge

$$V_m = \left[\frac{1}{2} - \frac{R}{(R + \Delta R_1) + R} \right] V_s \approx \left(\frac{\Delta R_1}{4R} \right) V_s \quad (\Delta R_1 \ll R)$$

(3) Sensitivity of output voltage variation to applied P

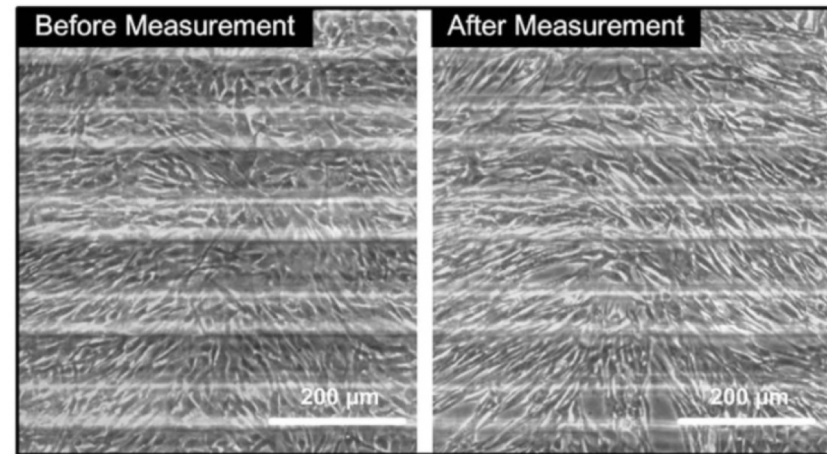
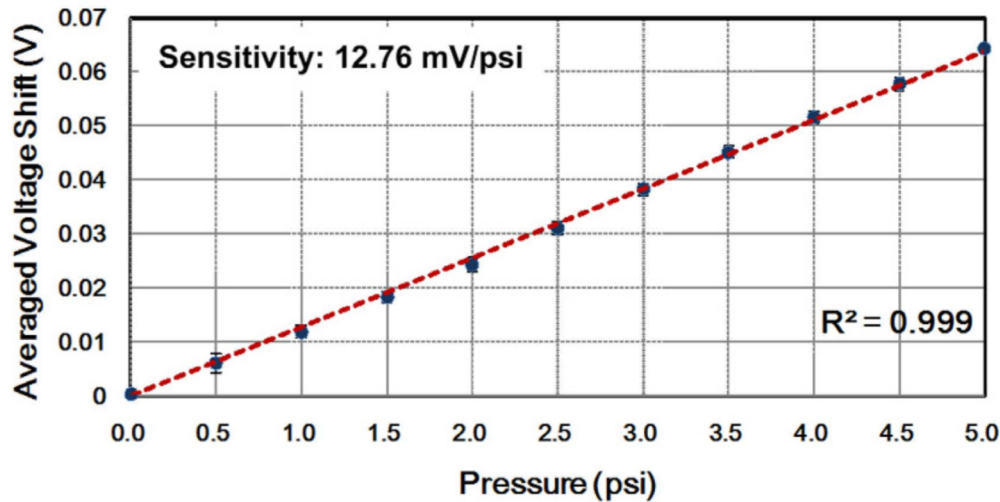
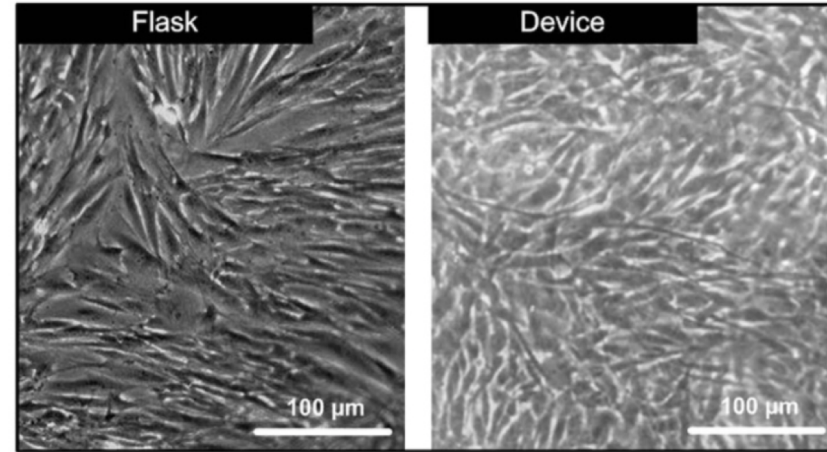
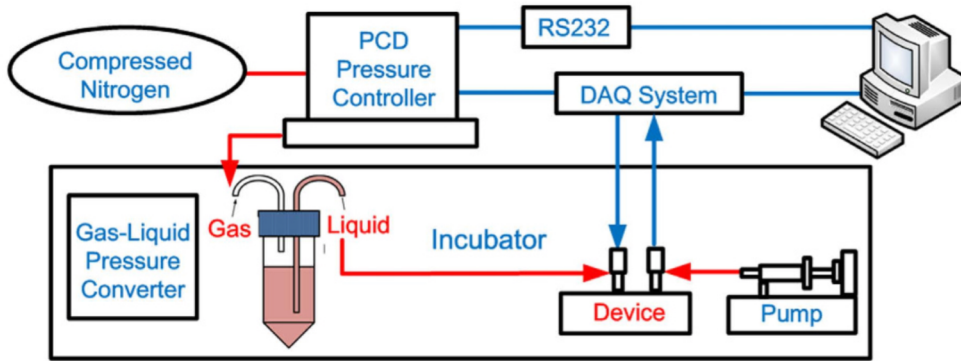
$$S_c \equiv \frac{\Delta V_m}{\Delta P} = \frac{L^4 V_s}{2880 H E_1 I(n)} \quad \left(n = \frac{E_2}{E_1} \right)$$

- ▶ **Pressure sensor embedded microfluidic device**: Measuring live cell layer in-plane elasticity
- ▶ **Bio-AFM**: Providing data of **cell thickness** and the **elastic modulus of PDMS** membrane
- ▶ **Timoshenko beam theory** needs to be utilized for the device with **thick** PDMS membrane

Measurement of in-plane elasticity of live cell layers



Microfluidic device development & mechanical model derivation

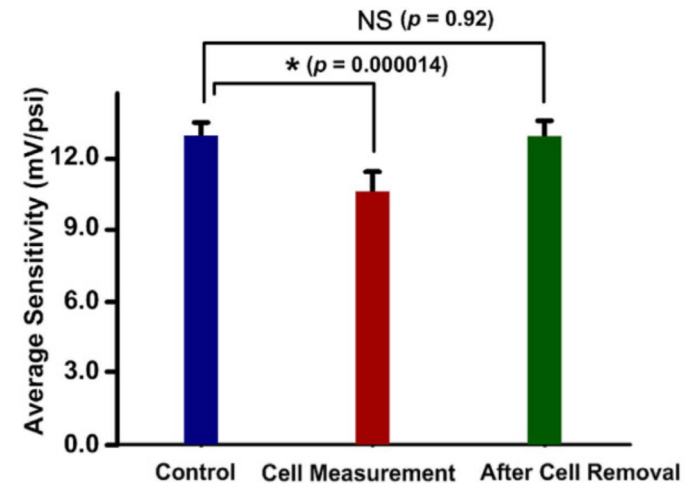
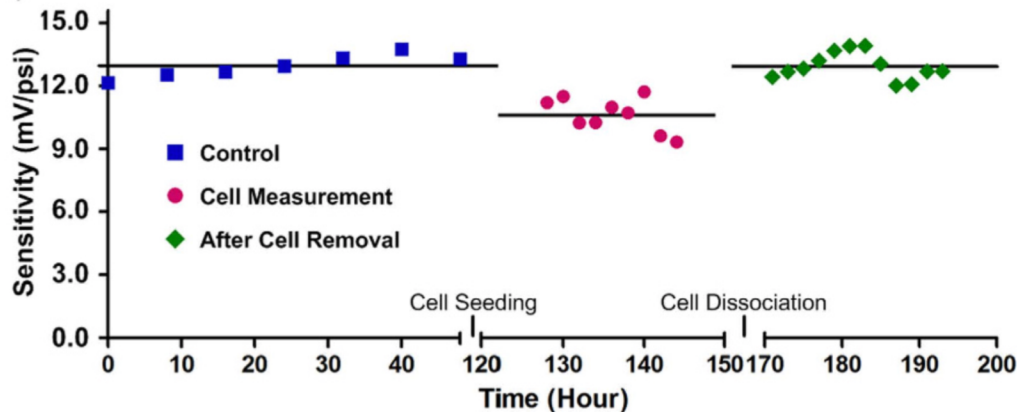
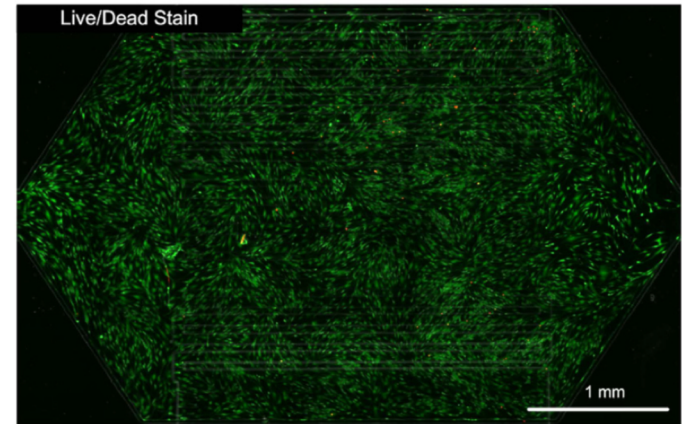
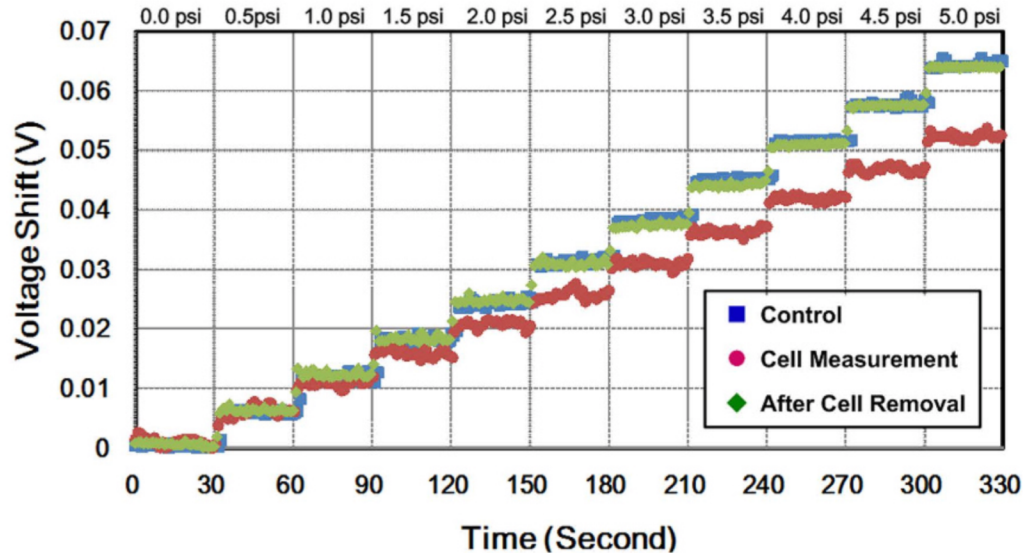


- ▶ Experimental setup for the **in-plane elasticity of cell layer** measurement
- ▶ **Pressure sensor calibration**: Raw data of output voltage shifts from the pressure sensor under various applied pressures (0 ~ 5 psi)
- ▶ Sensitivity of output voltage variation to applied P is obtained by **Linear regression of the results**.

Measurement of in-plane elasticity of live cell layers



Microfluidic device development & mechanical model derivation

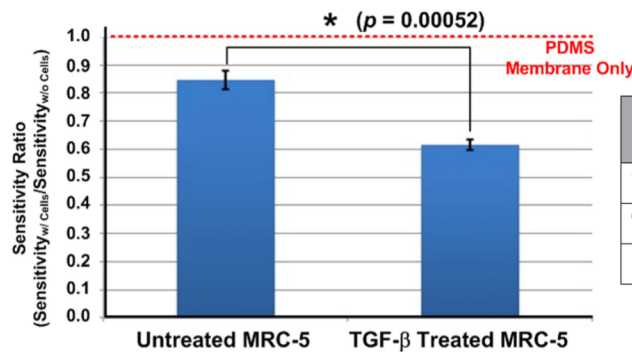
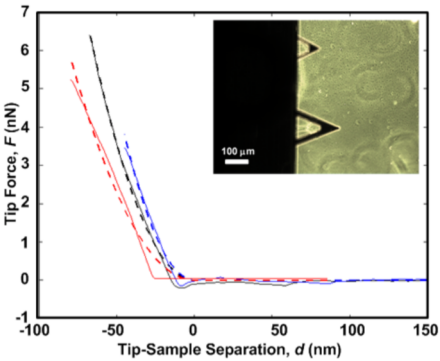
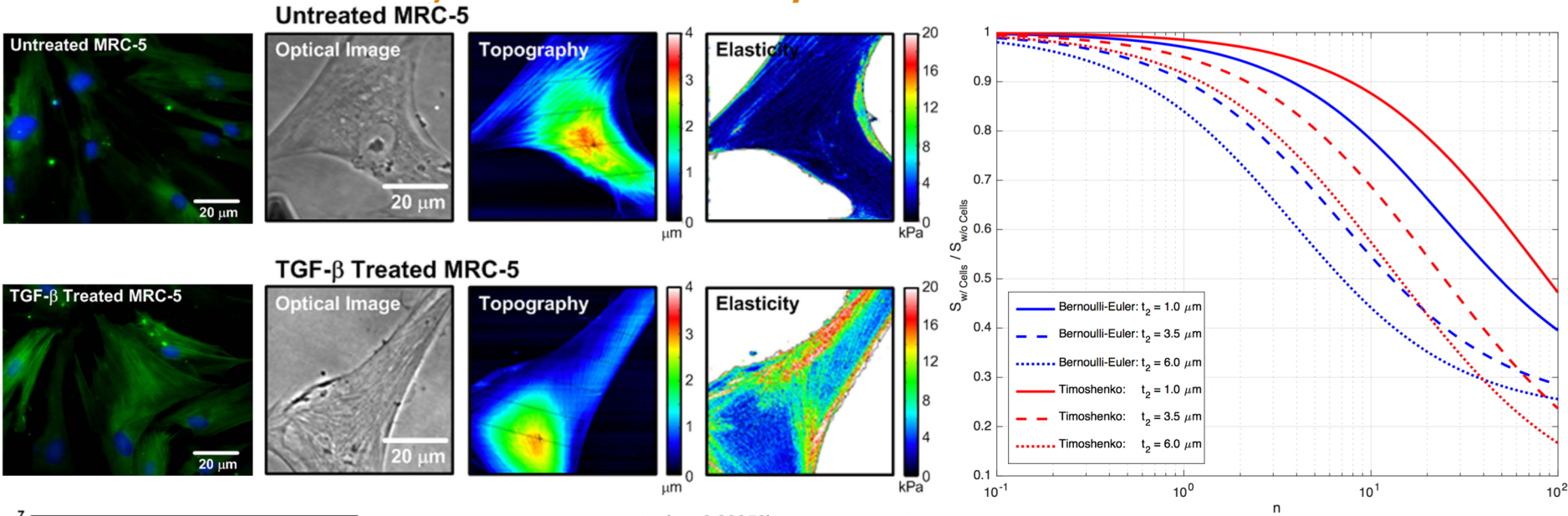


- ▶ Raw data of output voltage shifts from the pressure sensor under various applied pressures.
- ▶ Sensitivity variation during a set of control experiment, cell measurement, and after cell removal.
- ▶ Comparison of the averaged sensitivities under the three experimental conditions.

Bio-AFM & in-plane elasticity of live cell layers



Bio-AFM measurement of untreated and TGF- β treated MRC-5 cells



	In-Plane Elasticity by Microfluidic Device	AFM
Untreated MRC-5 (A)	6.38 ± 0.22 MPa	4.00 ± 1.34 kPa
TGF- β Treated MRC-5 (B)	33.78 ± 0.65 MPa	9.46 ± 0.71 kPa
(B)-(A)/(A)	429.3%	136.2%

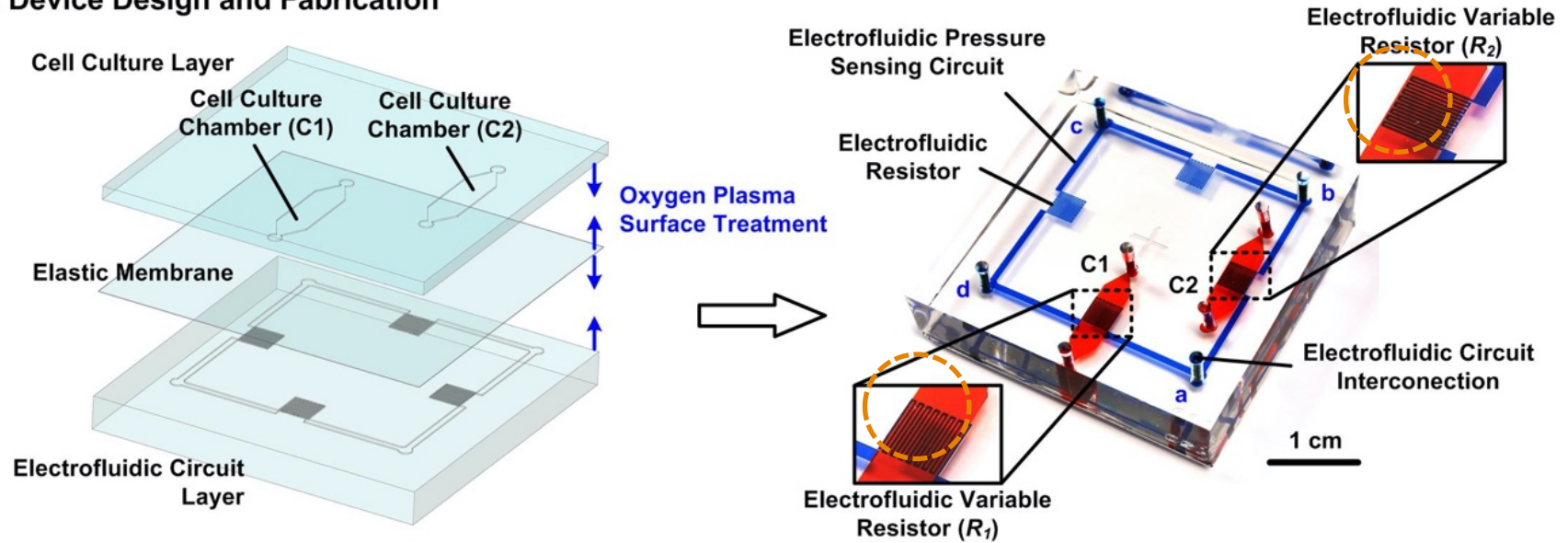
- ▶ Young's modulus measured in **normal direction**: Cell **membrane** elasticity & enclosed **cytoplasm**
- ▶ Young's modulus measured in **in-plane direction**: Cell elasticity of **cytoskeleton** including microfilaments, intermediate filaments & microtubules
- ▶ Elasticity **anisotropy** of MRC-5 cells: In-plane elasticity directly affects physiological activities of **vasodilation** and **lung expansion** due to **physically transformation** (fibroblast to myofibroblast)

Measurement of anisotropic elasticity of live cell layers

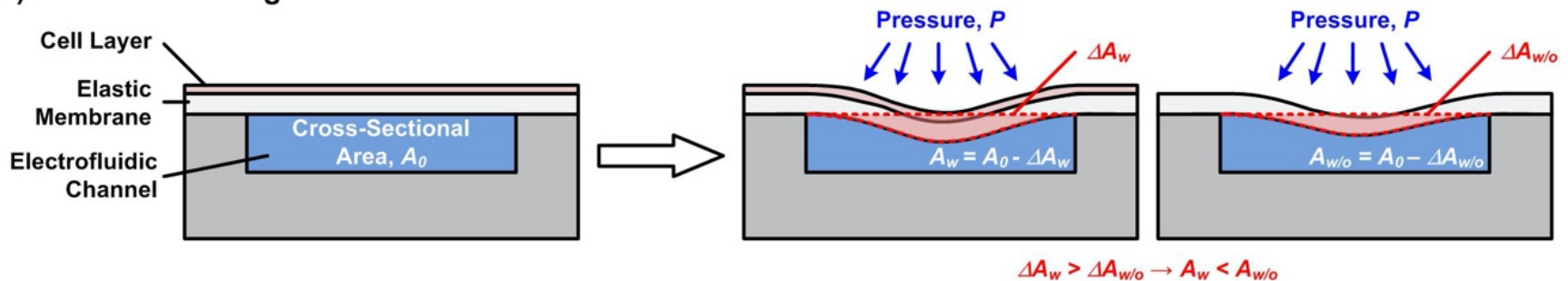


Microfluidic device development & mechanical model derivation

(a) Device Design and Fabrication



(b) Pressure Sensing Electrofluidic Variable Resistor



- ▶ A **microfluidic device** with the embedded electrofluidic pressure sensors for **measuring anisotropic elasticity of endothelial cells**
- ▶ Operation principles of the **microfluidic pressure sensor** for the cell elasticity characterization

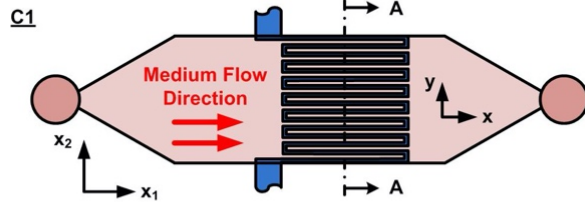
Measurement of anisotropic elasticity of live cell layers



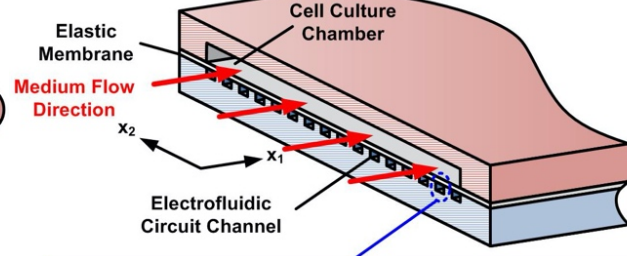
Microfluidic device development & mechanical model derivation

(c) Arrangement of Electrofluidic Variable Resistors

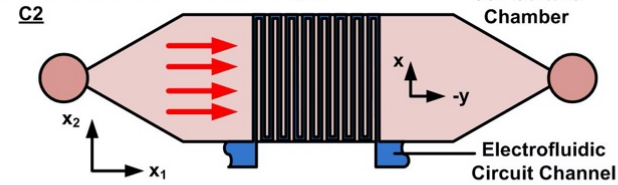
Electrofluidic Variable Resistor (R_{\perp}):



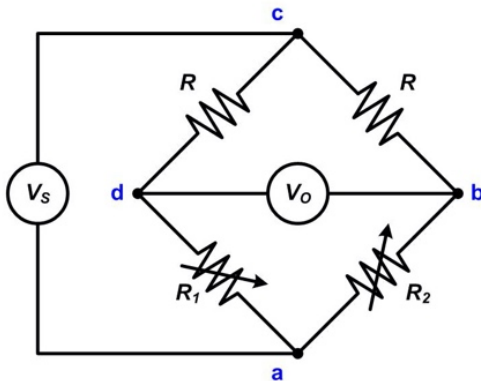
A-A Cross-Section:



Electrofluidic Variable Resistor (R_{\parallel}):

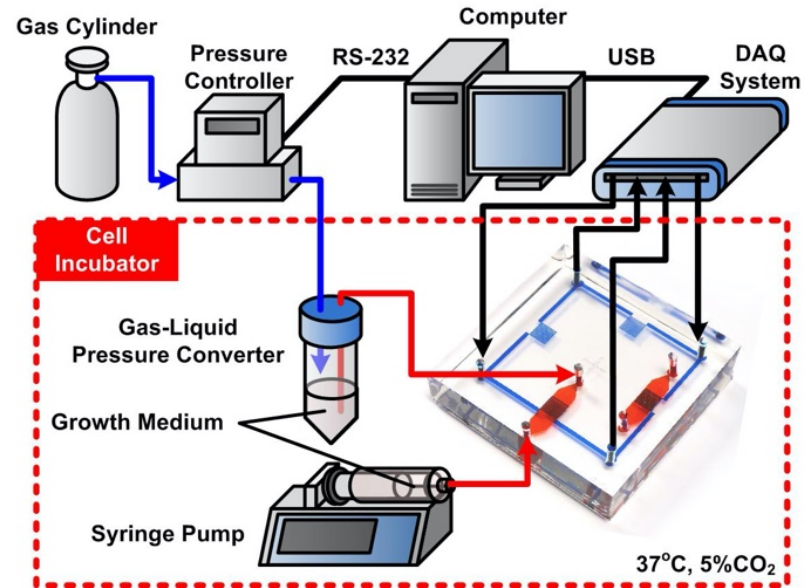


(d) Equivalent Electrical Circuit



V_s : Voltage source
 V_o : Voltage output
 R_1, R_2 : Pressure Sensing Variable Resistors
 R : Constant Resistors

(e) Experimental Setup

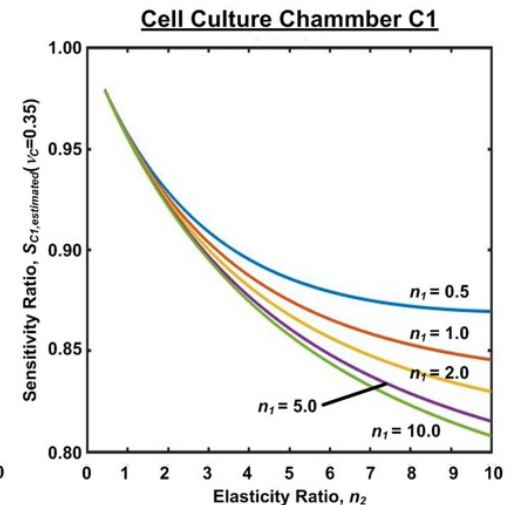
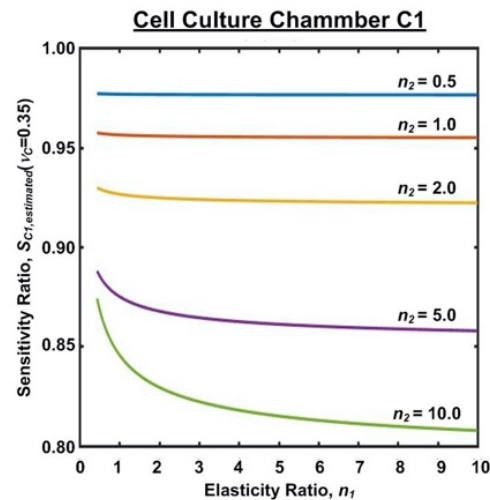
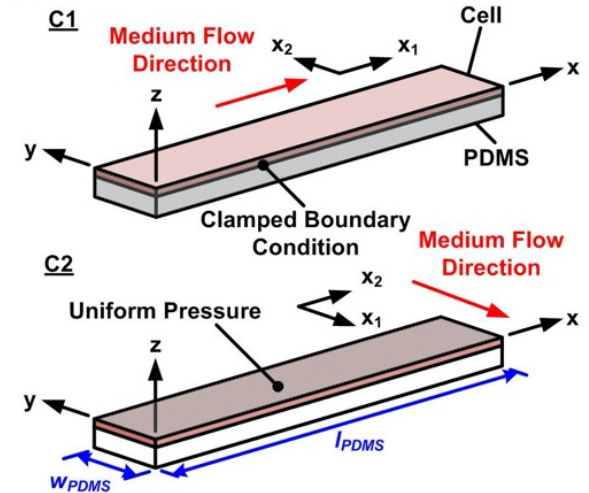
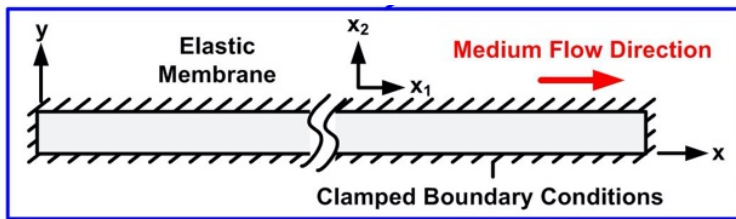
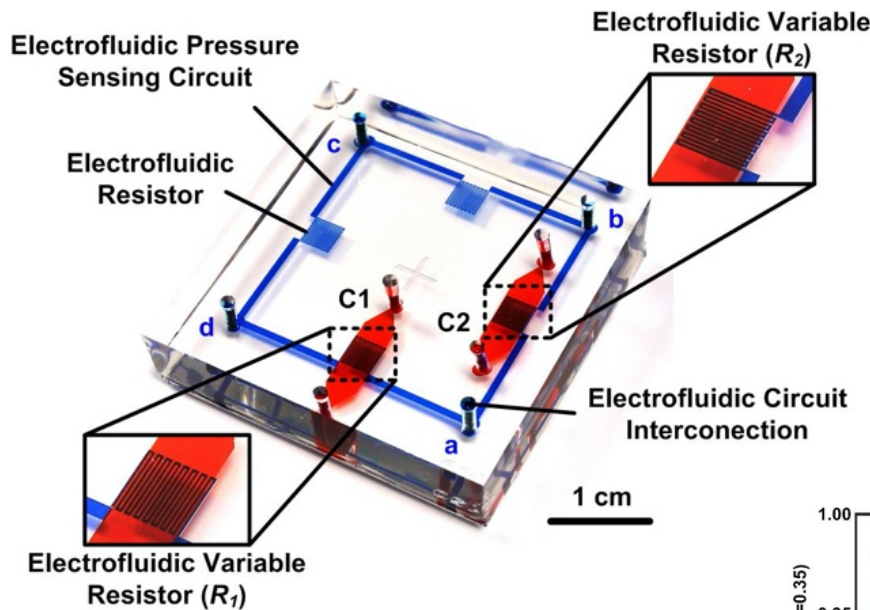


- ▶ Arrangement of the pressure sensors to measure the **transverse cell elasticities**
- ▶ Diagram of the experimental setup for the **elasticity measurement**



Measurement of in-plane elasticity of live cell layers

Microfluidic device development & mechanical model derivation



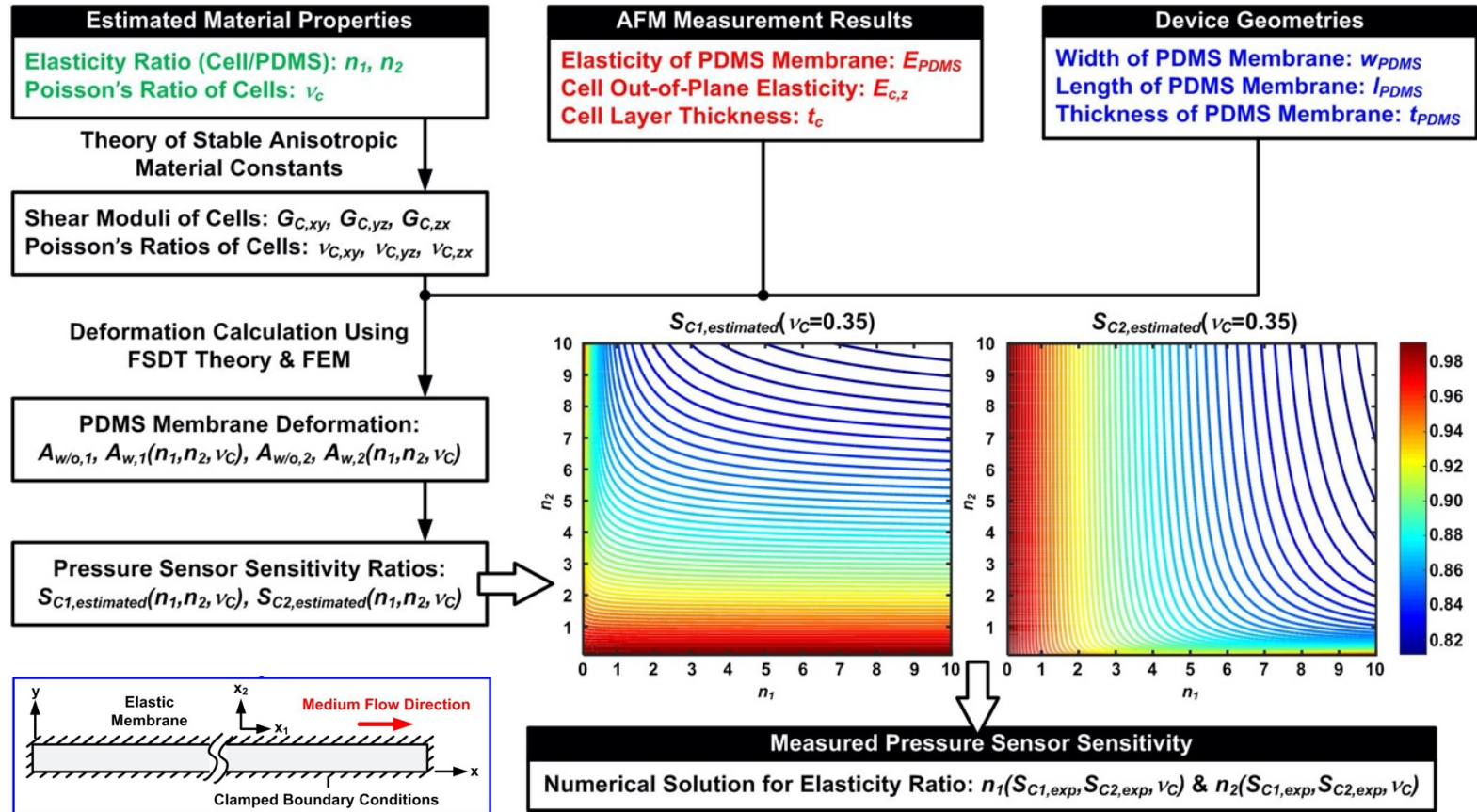
- ▶ The **theoretical mechanics model** constructed for the **cell elasticity** estimation.
- ▶ The theoretically derived results for the **sensitivity ratios** under **various elasticity ratio** combinations for the cell culture C1.

Measurement of in-plane elasticity of live cell layers



Microfluidic device development & mechanical model derivation

Material Property Estimation Process

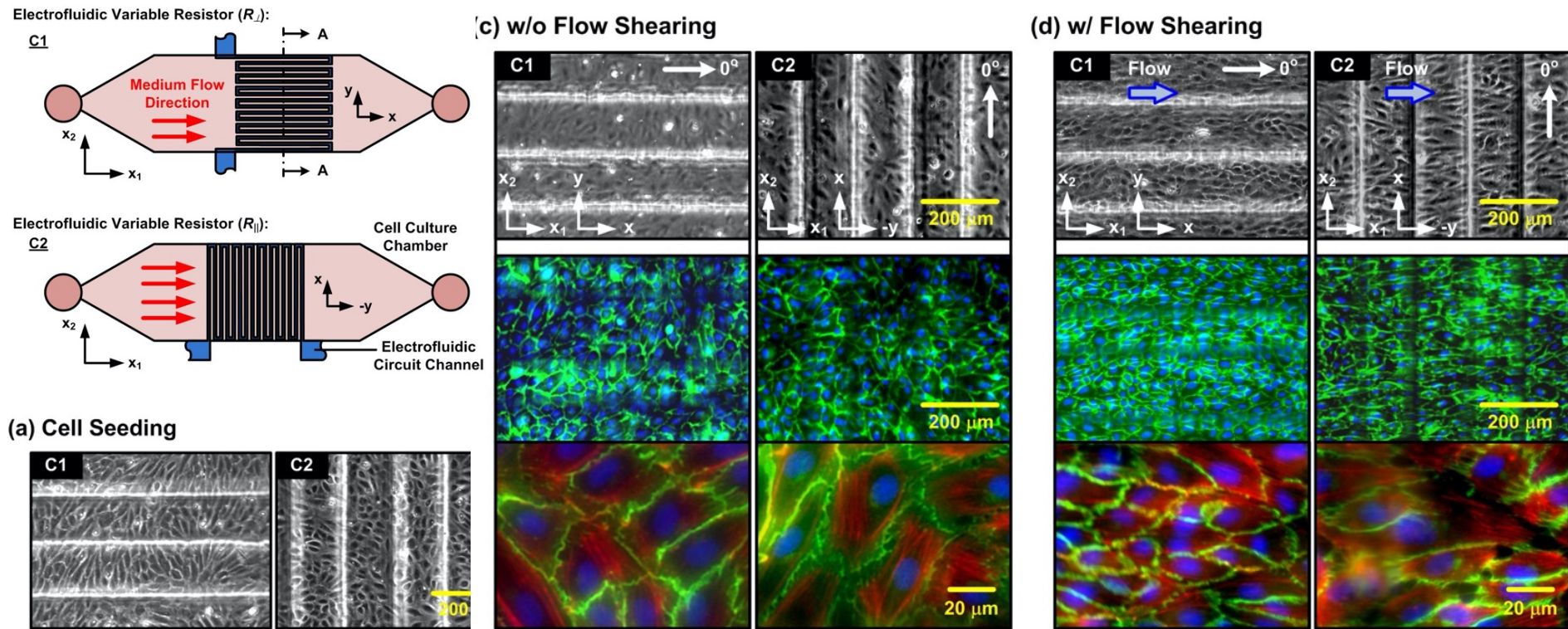


- ▶ The flowchart of the cell transverse elasticity estimation process taking advantage of the experimental data obtained in AFM analysis and pressure sensor-embedded microfluidic device measurement results.
- ▶ The elasticity calculation process is constructed based on the FSDT theory and FEM analysis.

Measurement of in-plane elasticity of live cell layers



Microfluidic device development & mechanical model derivation



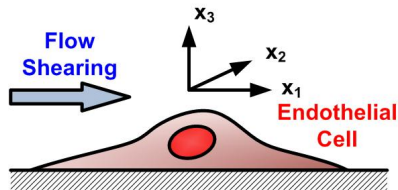
- ▶ The brightfield microscopic images of the **HUVECs** seeded in the **microfluidic device** after the cell seeding and attachment.
- ▶ The brightfield and fluorescence images of the **HUVECs** which are **stained**: blue for **nuclei**, green for **VE-cadherin**, and red for **F-actin**.



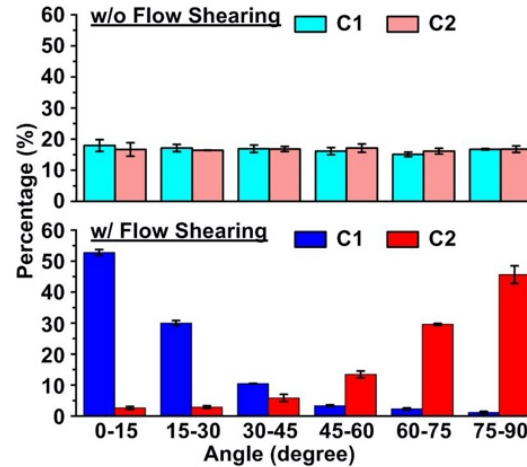
Measurement of in-plane elasticity of live cell layers

Microfluidic device development & mechanical model derivation

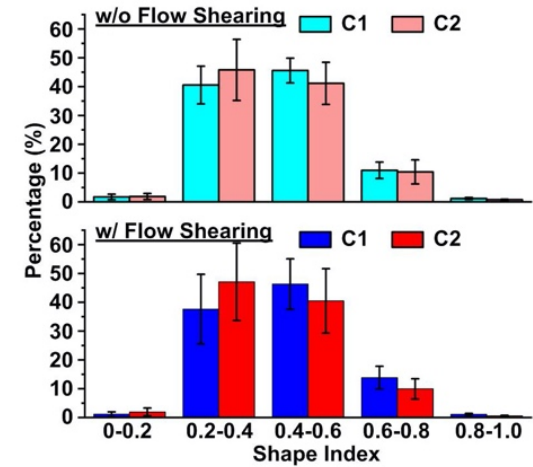
(c) Elasticity Comparison



(e) Cell Alignment

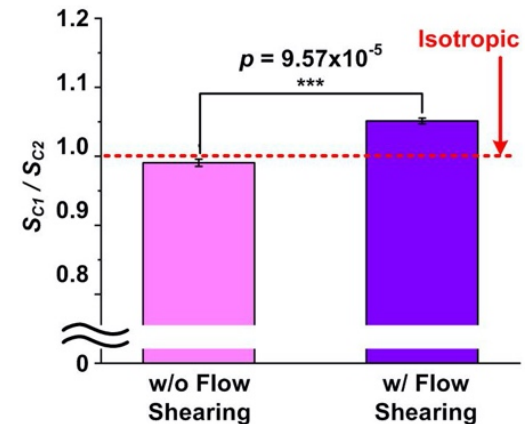


(f) Cell Morphology



$$\text{Sensitivity Ratio (S)} = \frac{\text{Sensitivity (w/ cells)}}{\text{Sensitivity (w/o cells)}}$$

	w/o Flow Shearing			w/ Flow Shearing		
	S_{C1}	S_{C2}	S_{C1} / S_{C2}	S_{C1}	S_{C2}	S_{C1} / S_{C2}
Experiment 1	0.886	0.889	0.997	0.895	0.848	1.055
Experiment 2	0.904	0.913	0.990	0.852	0.814	1.047
Experiment 3	0.905	0.918	0.986	0.878	0.835	1.051
Mean	0.898	0.907	0.991	0.875	0.832	1.051
SEM	6.17×10^{-3}	8.95×10^{-3}	3.14×10^{-3}	1.25×10^{-2}	9.91×10^{-3}	2.53×10^{-3}



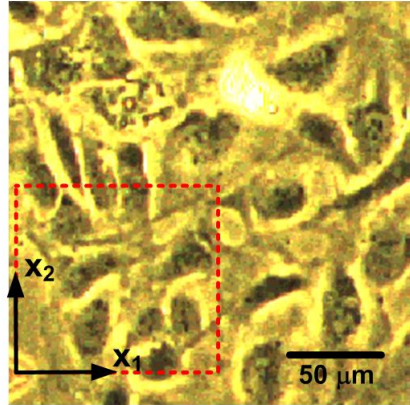
- ▶ Cell **alignment** and **morphology** analysis results from the microscopic images. (The flow direction is defined as 0 degree.)
- ▶ The summarized **sensitivity ratios** calculated from the experiments **with** and **without** the HUVECs cultured in the devices.



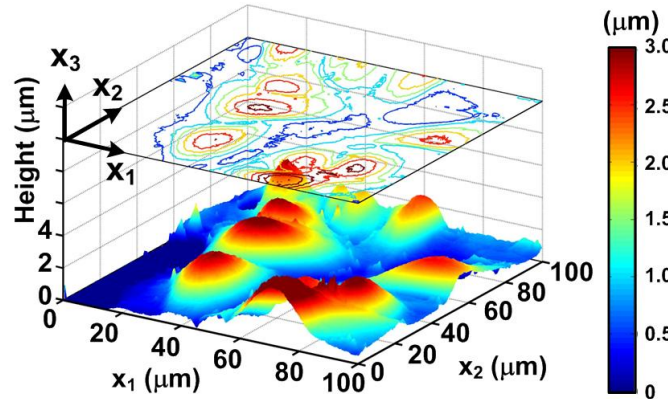
Measurement of in-plane elasticity of live cell layers

Microfluidic device development & mechanical model derivation

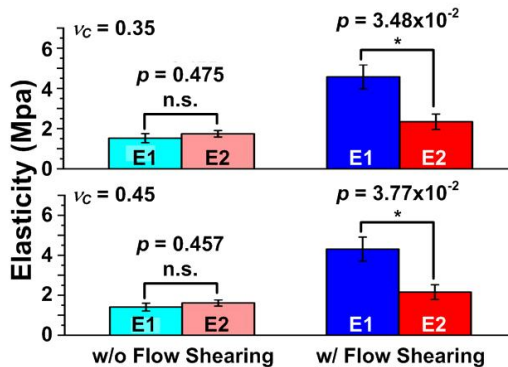
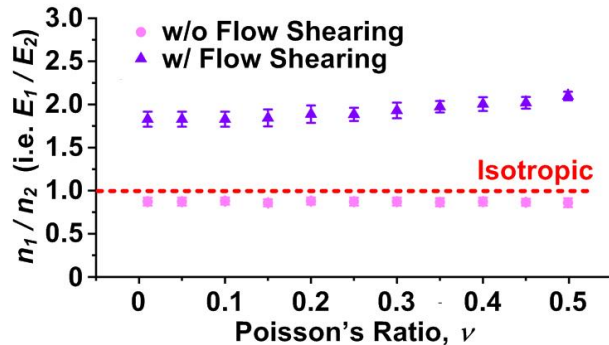
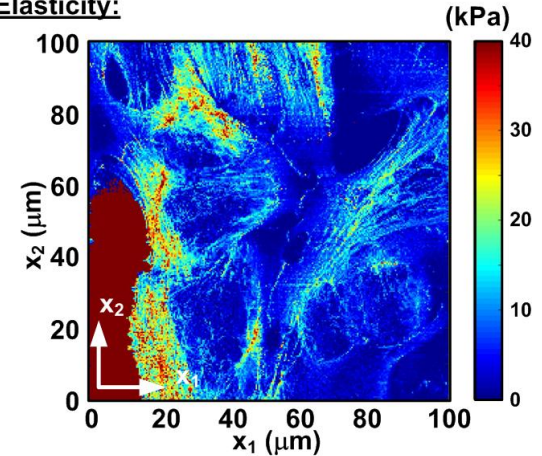
(a) AFM Measurement



Topography:



Elasticity:

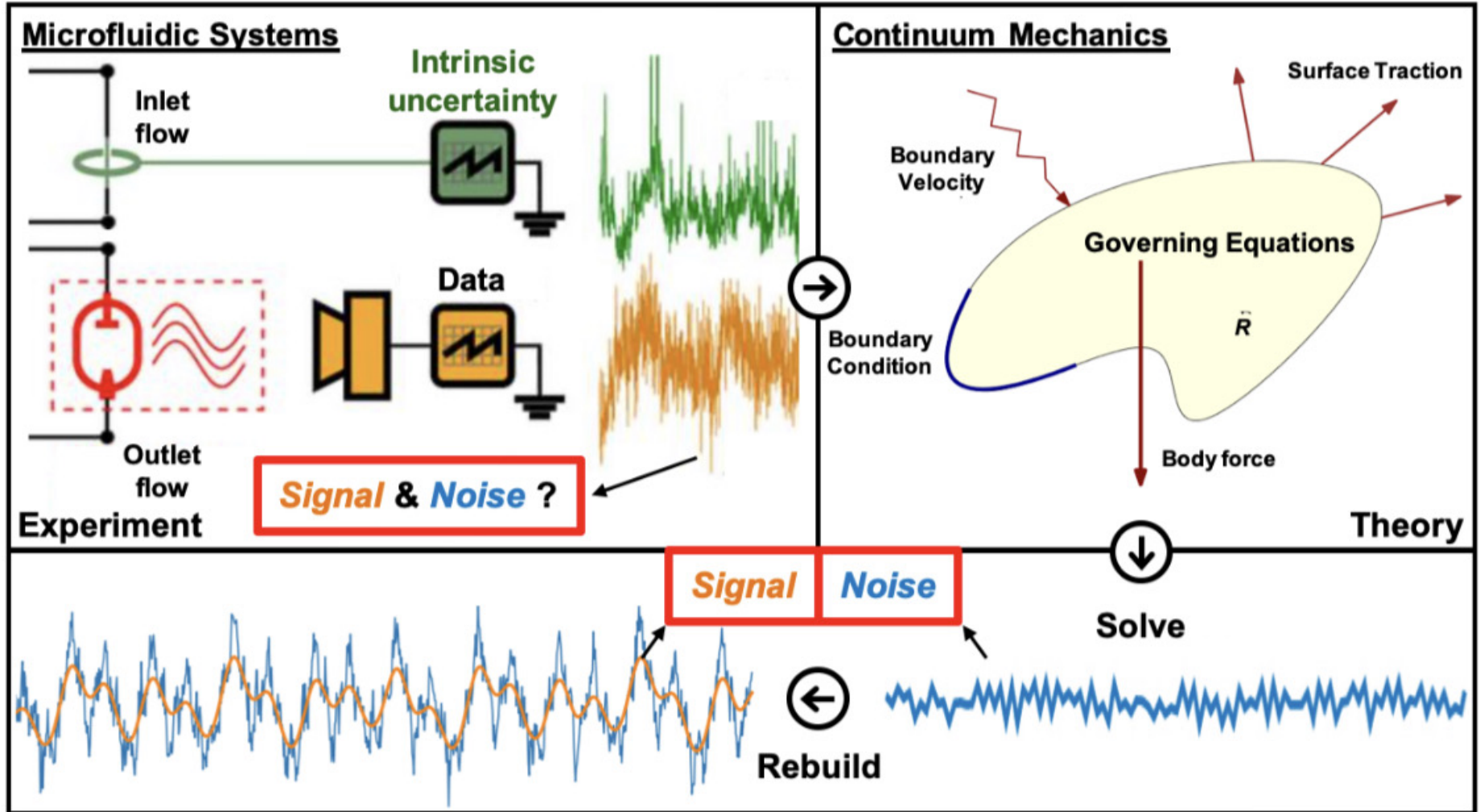


	w/o Flow Shearing		w/ Flow Shearing	
	$\nu = 0.35$	$\nu = 0.45$	$\nu = 0.35$	$\nu = 0.45$
E_1	1.52 ± 0.23 MPa	1.41 ± 0.20 MPa	4.57 ± 0.60 MPa	4.31 ± 0.60 MPa
E_2	1.74 ± 0.16 MPa	1.61 ± 0.16 MPa	2.34 ± 0.38 MPa	2.16 ± 0.37 MPa
E_3	9.39 ± 0.76 kPa (AFM Measurement)			

- ▶ The microscopic and **AFM topographic images** of the HUVECs cultured in a Petri-dish.
- ▶ **Cell transverse elasticities** in different directions are estimated for different Poisson's ratios.
- ▶ Summary of experimental results obtained in the **AFM analysis and microfluidic device measurements** based on the developed process without and with flow shearing.



Motivation – Measurement noise reduction for Stokes flow



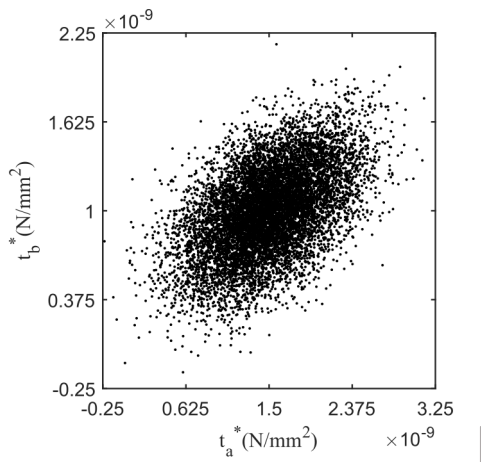
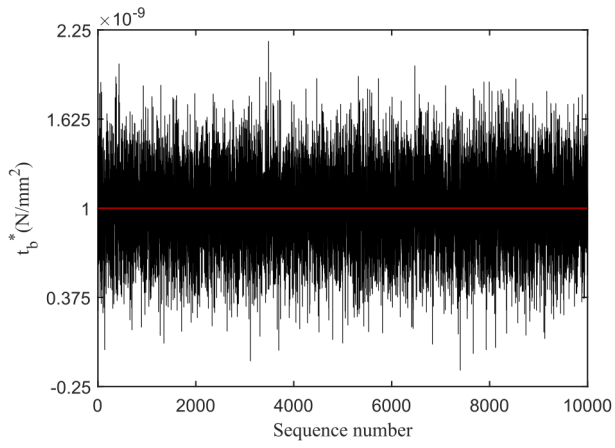
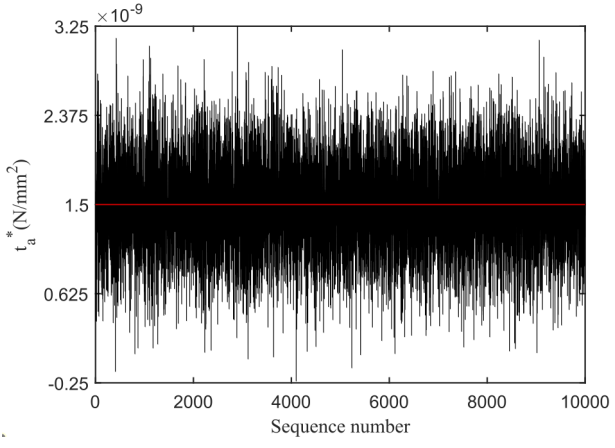
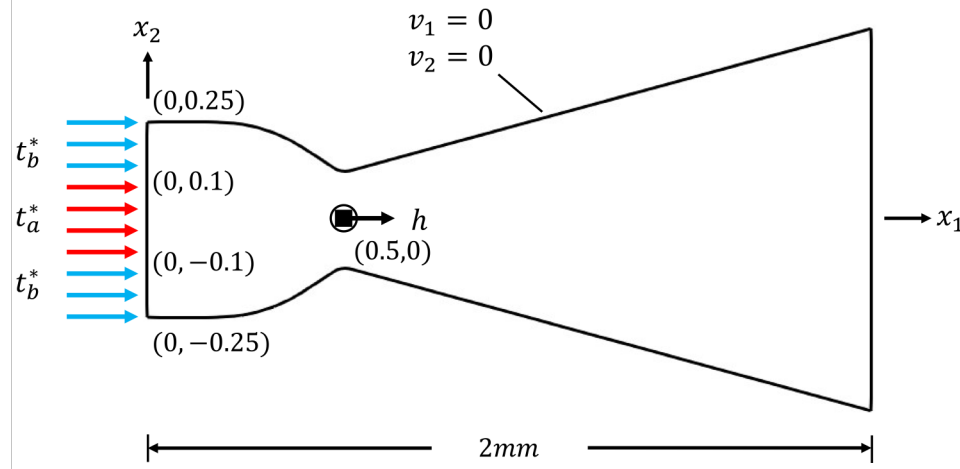


Numerical examples – CD nozzle

Uncertainty conditions: t_a^* & t_b^*
 Observation pt: h (0.5, 0), in horizontal dir.

Length: 2 (mm)
 Inlet diameter: 0.5 (mm)
 t_a^* : 1.5 (mPa)
 t_b^* : 1 (mPa)
 Fluid: water, at 20°C
 Dynamic viscosity: 1×10^{-9} (N · s/mm²)
 Kinematic viscosity: 1 (mm²/s)

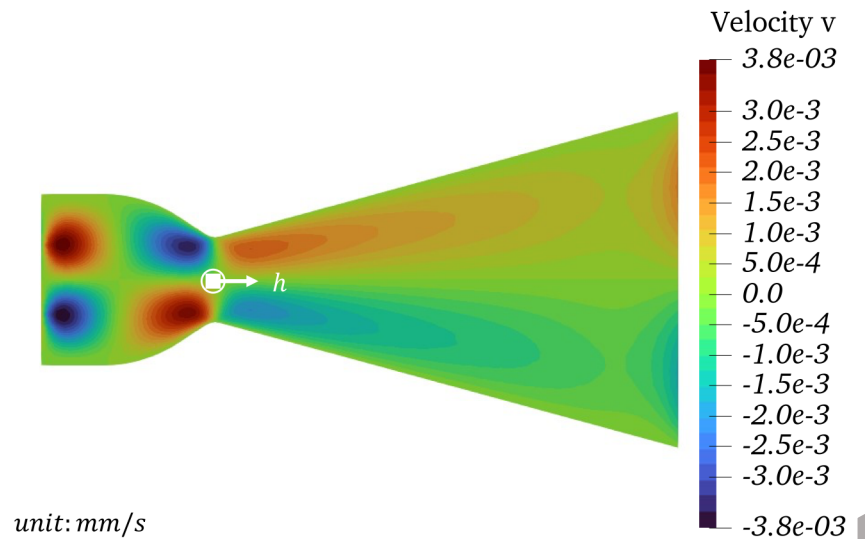
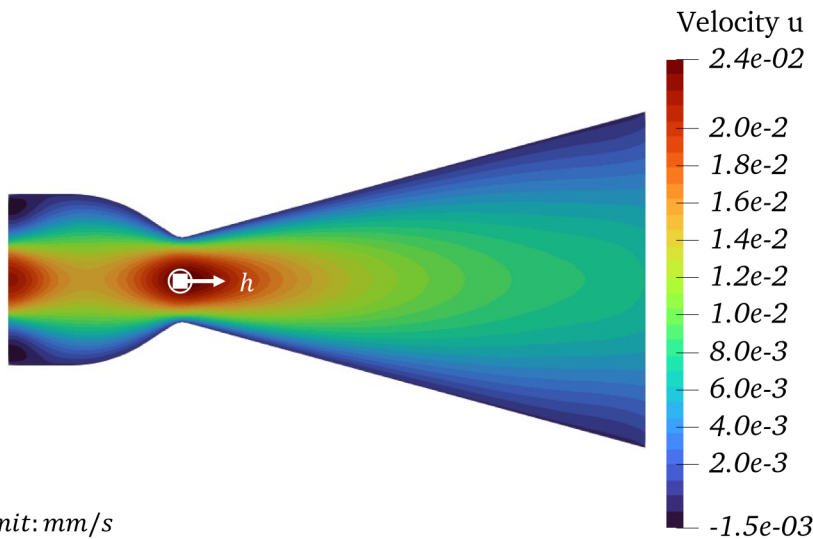
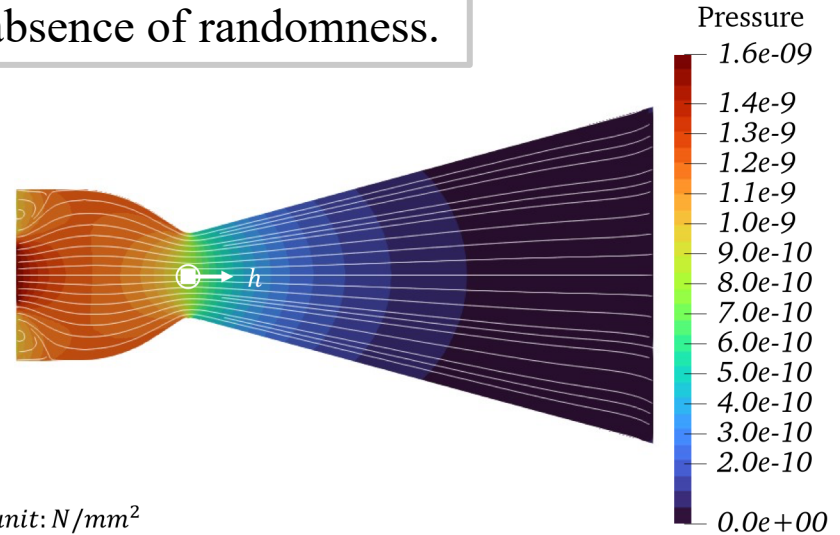
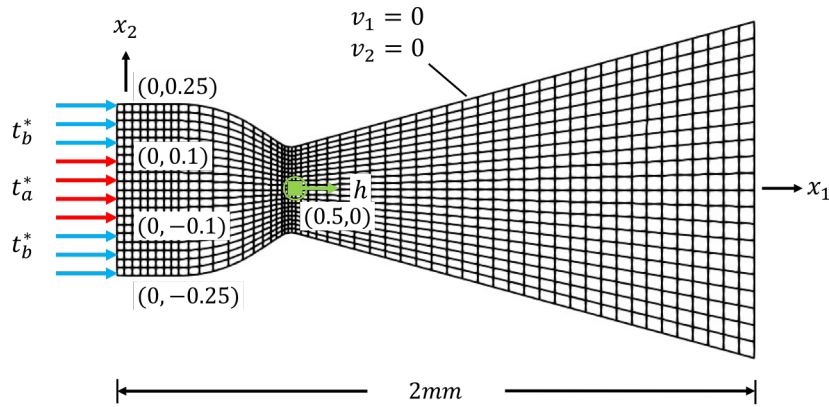
$\sigma_{t_a^*} = 0.45$ (mPa)
 $\sigma_{t_b^*} = 0.3 \times$ (mPa)
 $\rho_{t_a^* t_b^*} = 0.5$





Numerical examples – CD nozzle

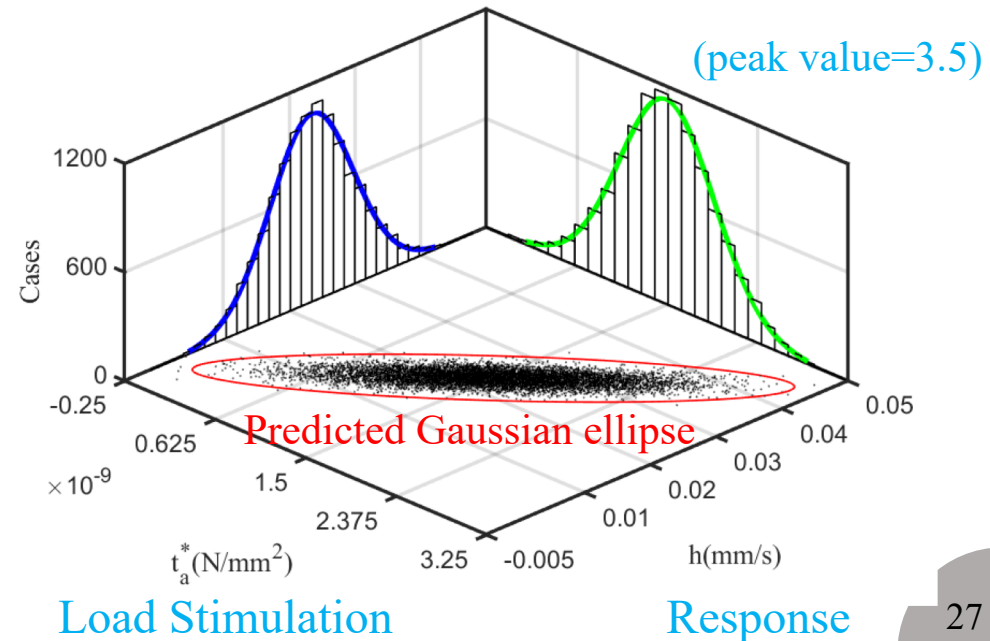
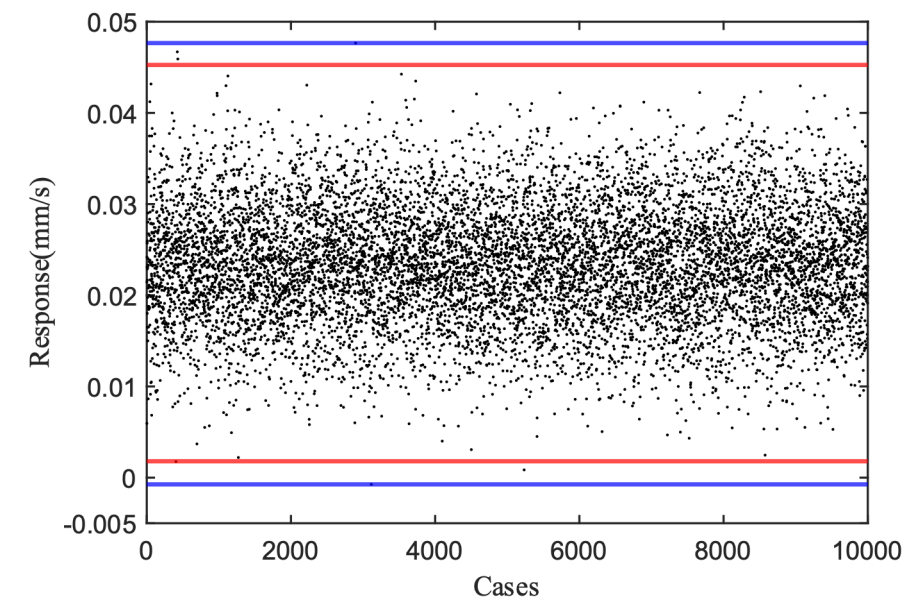
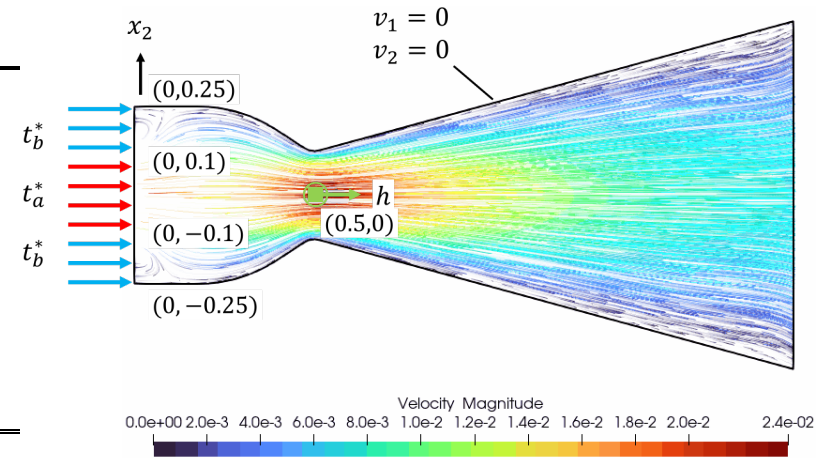
The computation result in the absence of randomness.





Numerical examples – CD nozzle

	Sampling test	FLRC	Error (%)
Response avg. (mm/s)	0.02345	0.02353	0.34
Response std. (mm/s)	0.006269	0.006209	0.95
Correlation coef. (h, t_a^*)	0.9419	0.9402	0.18
Pos. peak response(mm/s)	0.04766	0.04526	10.22
Neg. peak response(mm/s)	-0.0007387	0.001797	10.82
	Pos. peak response	Neg. peak response	
Fail prediction(%)	0.03	0.02	



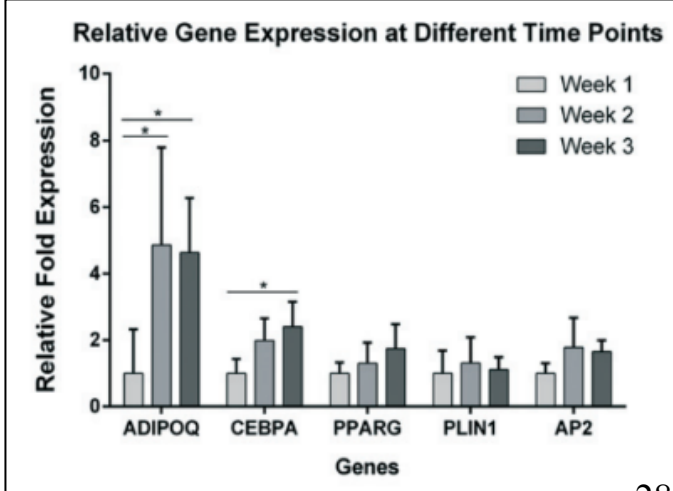
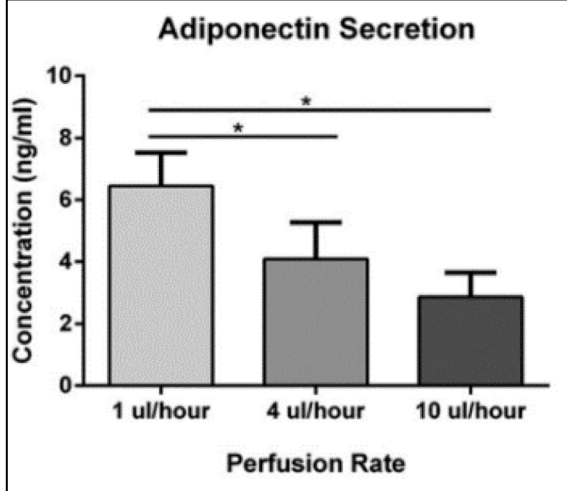
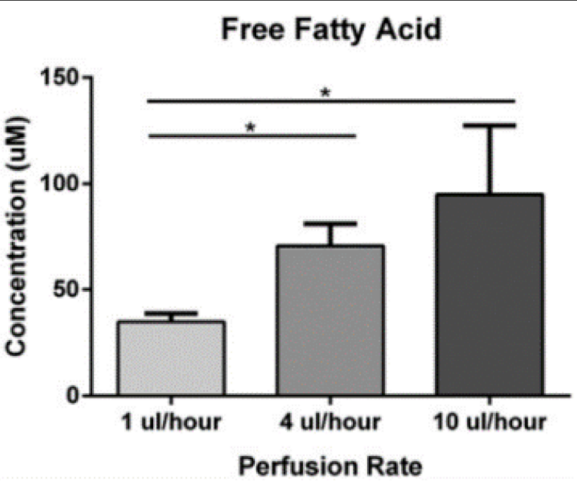
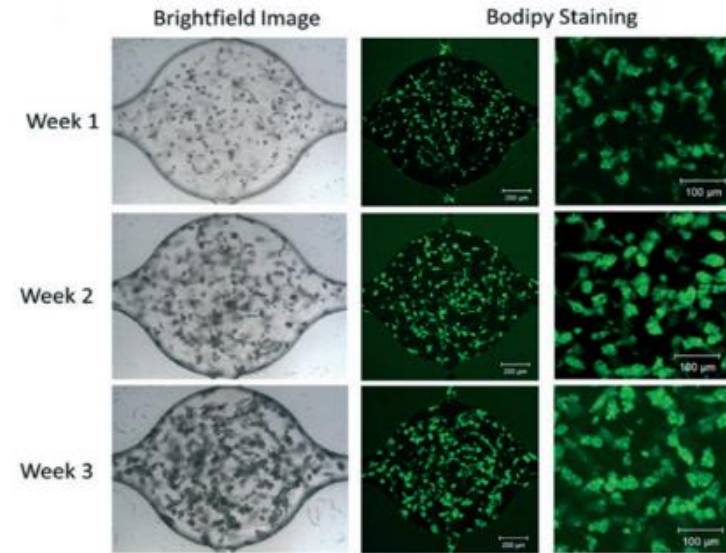
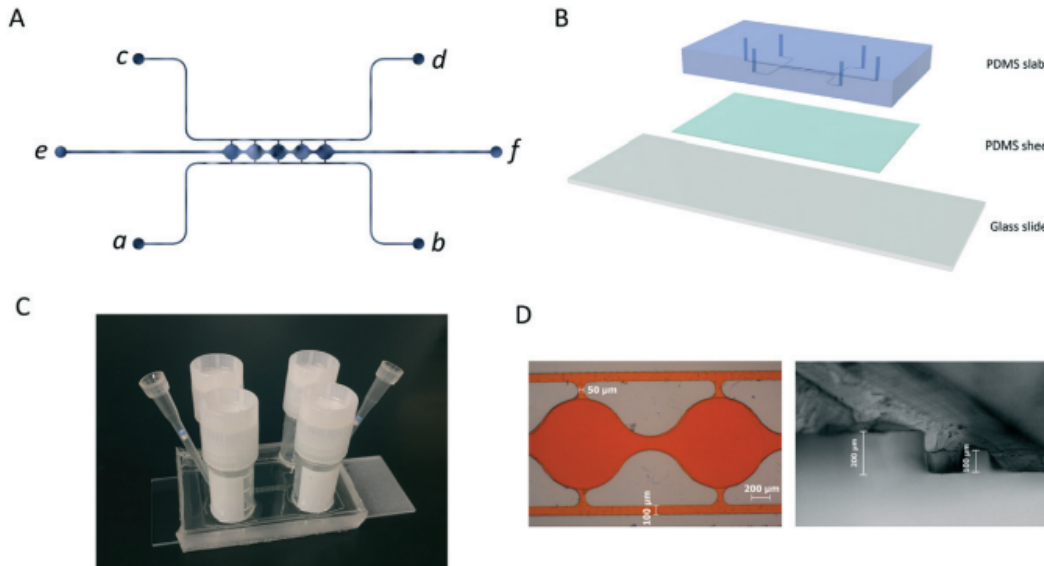


Numerical examples – Microfluidic chamber

A 3D human adipose tissue model within a microfluidic device

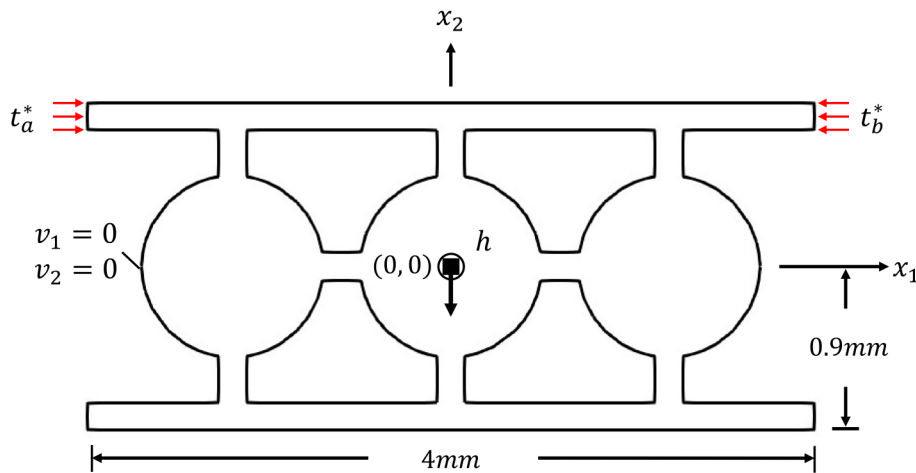
Lab on a Chip 2021 Vol. 21 Issue 2 Pages 435-446

Investigating the effects of shear stress at different flow rates in a cell culture chamber on cellular physiological responses.





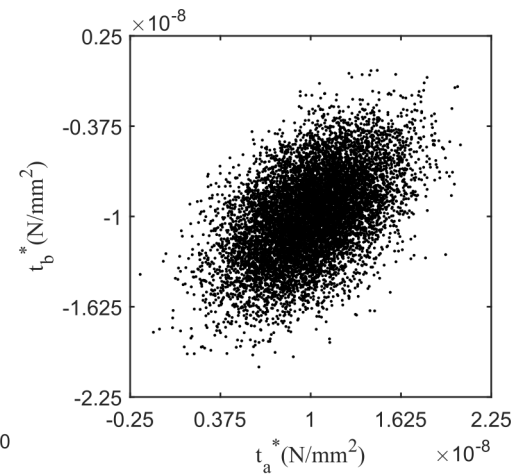
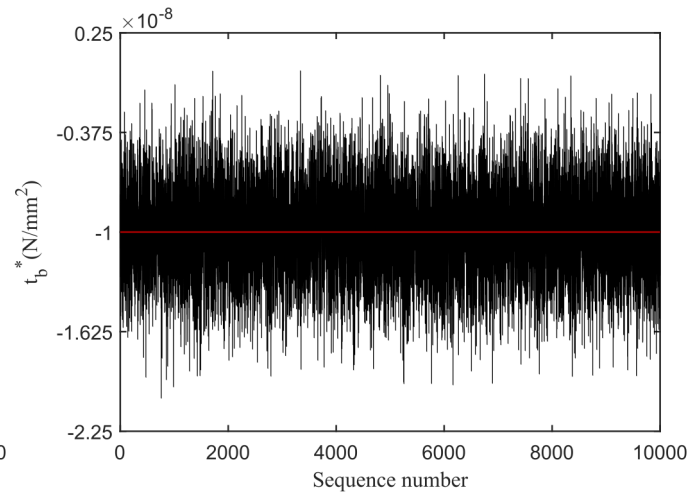
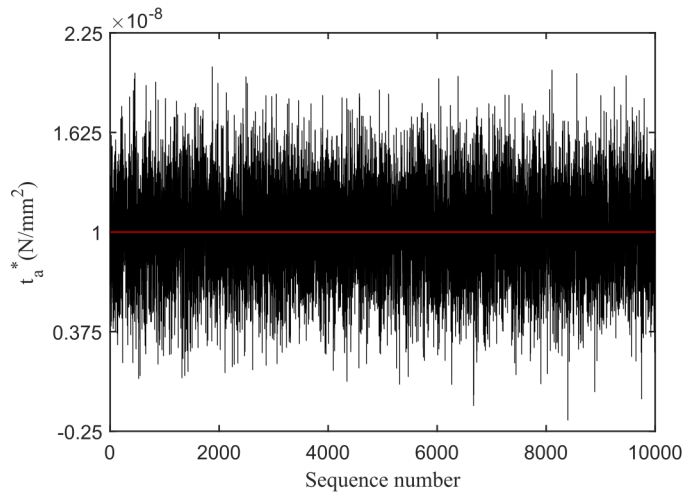
Numerical examples – Microfluidic chamber



Uncertainty conditions: t_a^* & t_b^*
Observation pt: $h(0, 0)$, in vertical dir.

Chamber diameter: 1 (mm)
Pipe diameter: 0.2 (mm)
 $t_a^* : 10$ (mPa) ; $t_b^* : -10$ (mPa)
Fluid : water, at 20°C
Dynamic viscosity: 1×10^{-9} (N · s/mm²)
Kinematic viscosity: 1 (mm²/s)

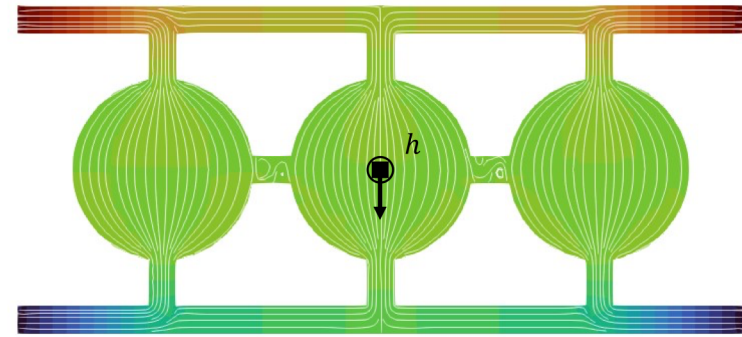
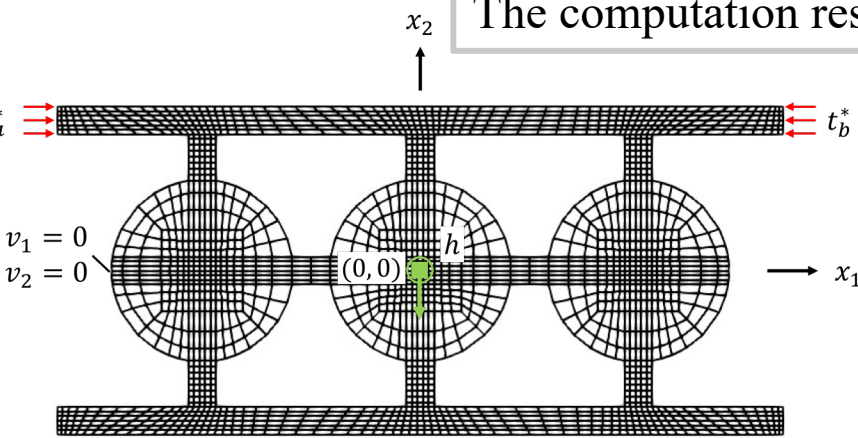
$\sigma_{t_a^*} \& \sigma_{t_b^*} = 3$ (mPa)
 $\rho_{t_a^* t_b^*} = 0.5$



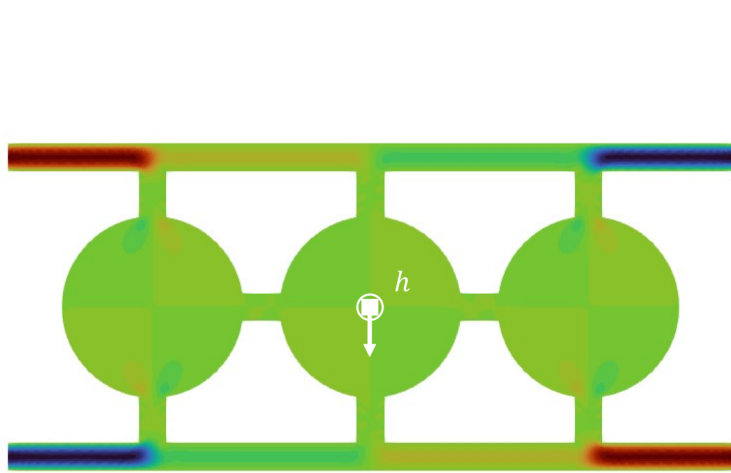
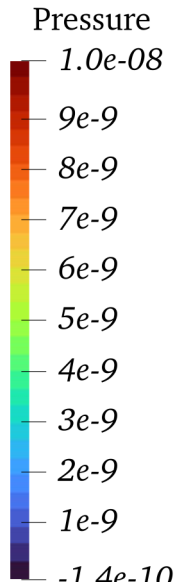


Numerical examples – Microfluidic chamber

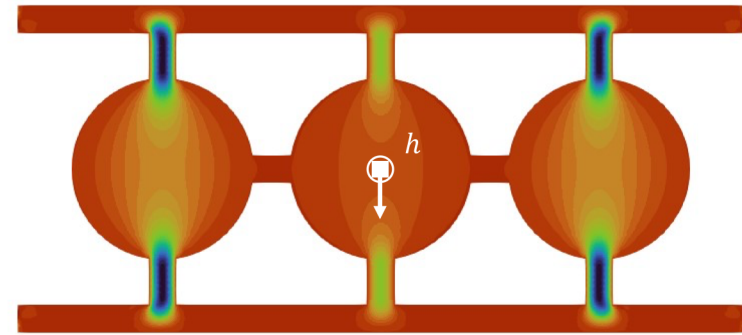
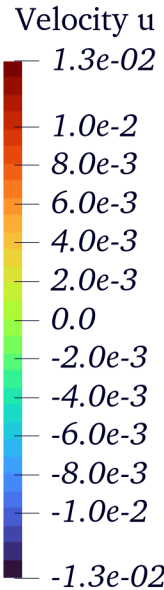
The computation result in the absence of randomness.



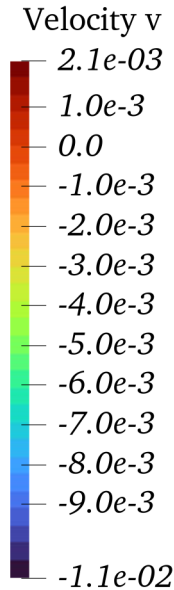
unit: N/mm^2



unit: mm/s



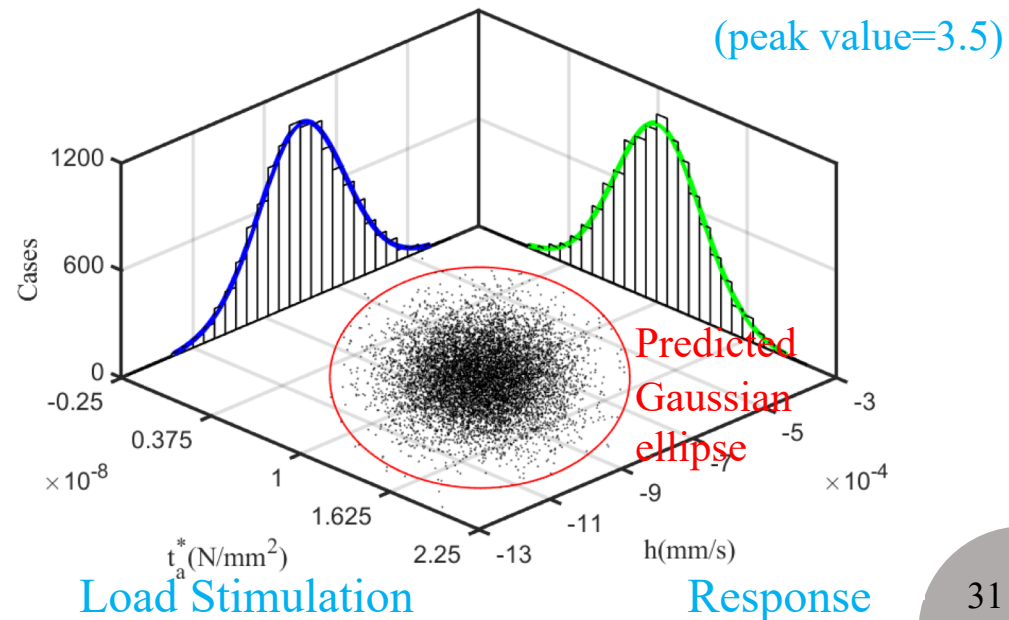
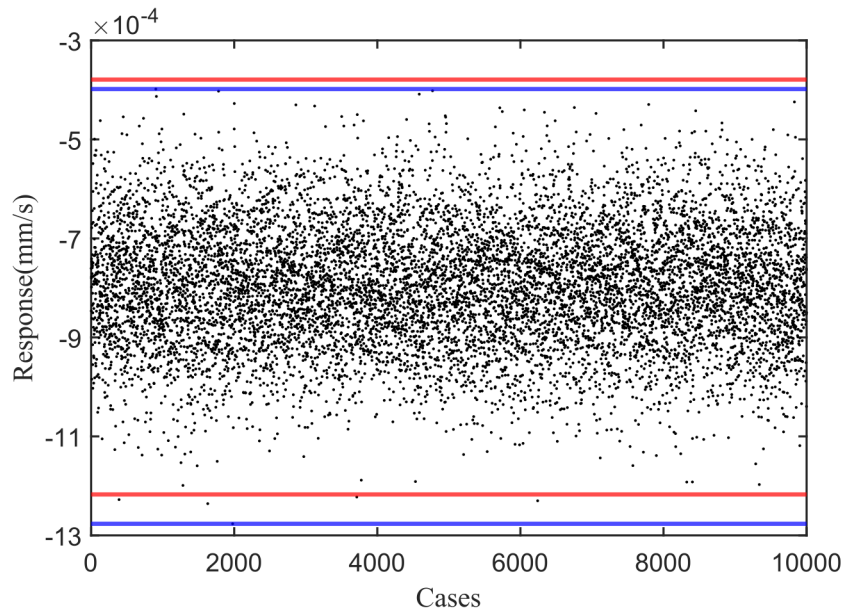
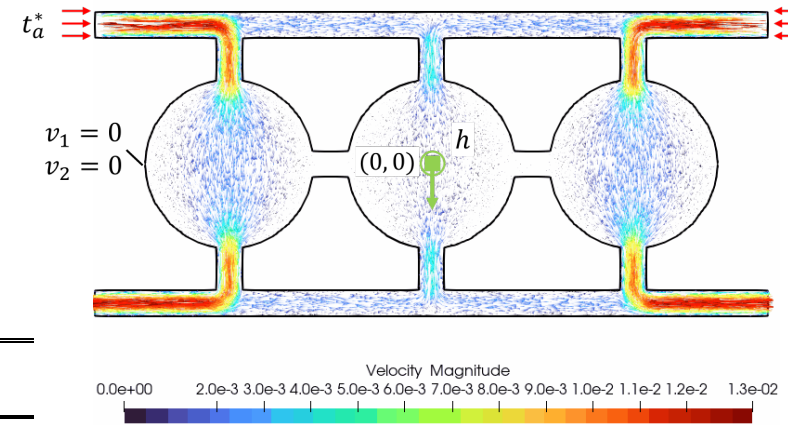
unit: mm/s





Numerical examples – Microfluidic chamber

	Sampling test	FLRC	Error (%)
Response avg. (mm/s)	-0.0007955	-0.0007982	0.34
Response std. (mm/s)	0.0001198	0.0001197	0.058
Correlation coef. (h, t_a^*)	-0.5014	-0.5005	0.17
Pos. peak response(mm/s)	-0.0003983	-0.0003792	2.40
Neg. peak response(mm/s)	-0.001277	-0.001217	7.45
	Pos. peak response	Neg. peak response	
Fail prediction(%)	0.00	0.05	



Noise reduction example – cavity flow

Marginal length: 1 mm ; Upper border BC: 1mm/s(x-dir.)
 SAE 80W-90 oil Dynamic viscosity: $1.36 \times 10^{-4} \text{ N} \cdot \text{s}/\text{mm}^2$
 Std. of simulation noise: 30% field maximum

$$\mathbf{h} = (\mathbf{I} + \mathbf{Q}^{-1} \tilde{\mathbf{A}}^T \Delta^{-1} \tilde{\mathbf{A}}) \hat{\mathbf{h}}$$

Noise reduce
(RMSE)(%)

Velocity $u(\text{mm}/\text{s})$

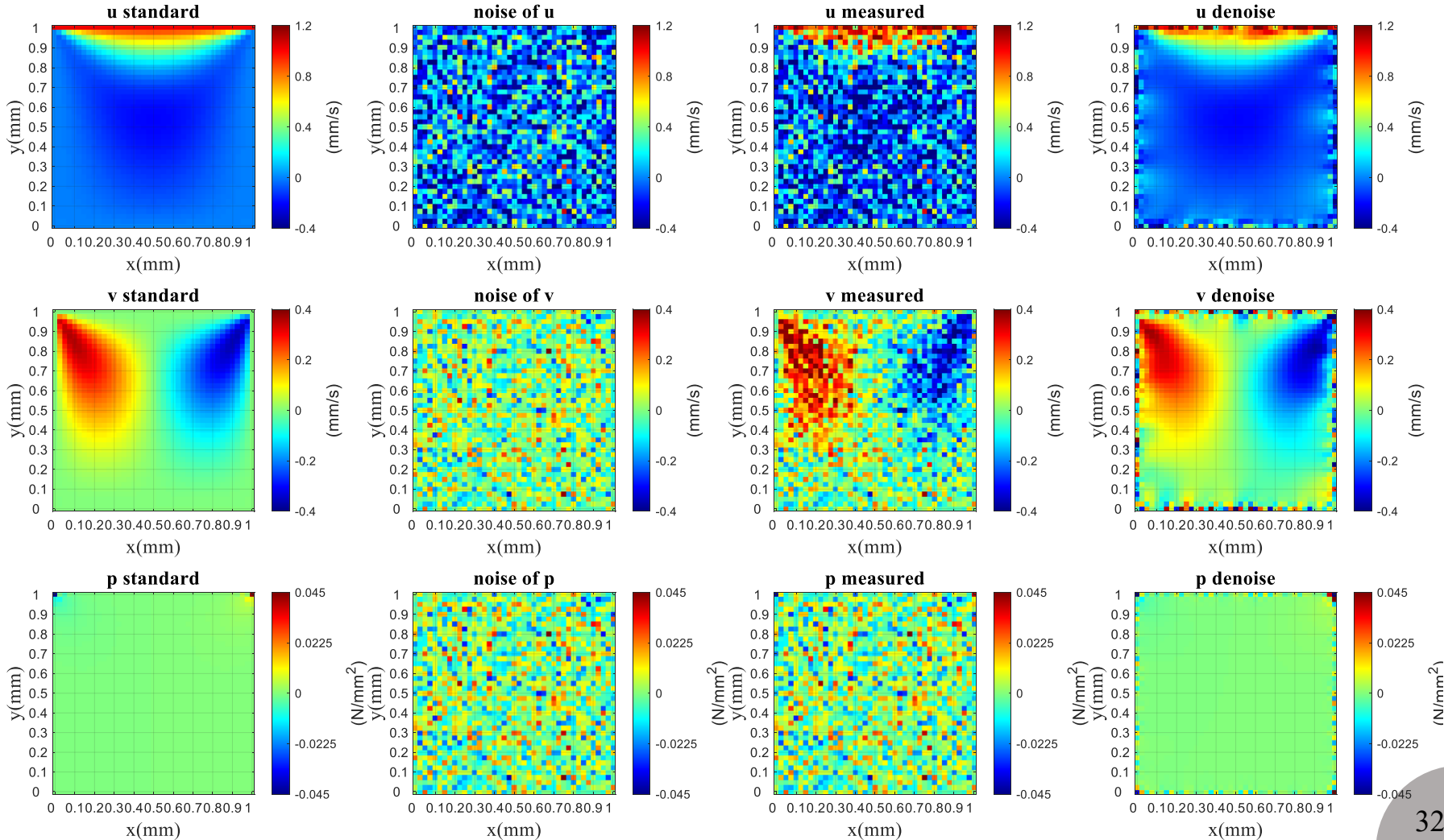
85.92

Velocity $v(\text{mm}/\text{s})$

73.68

Pressure (N/mm^2)

97.70





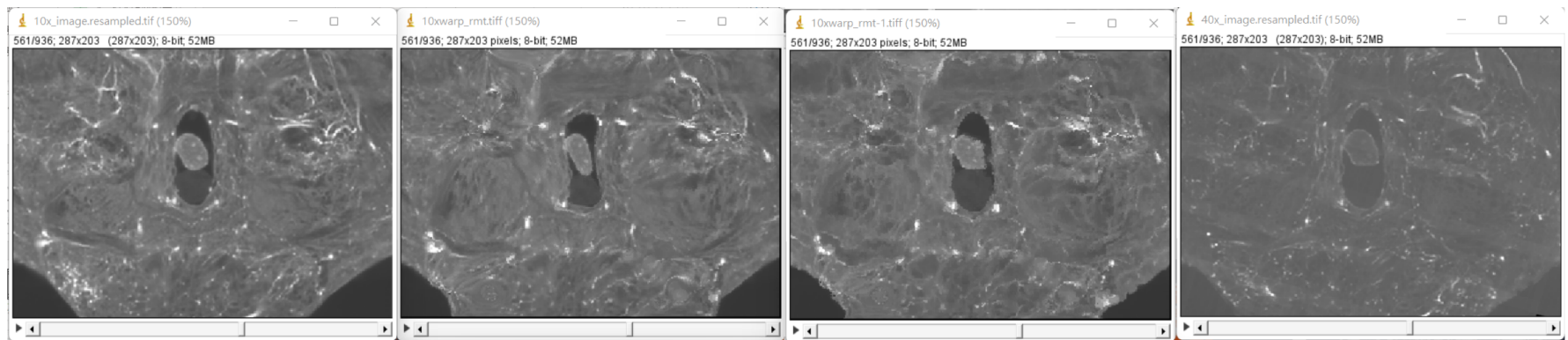
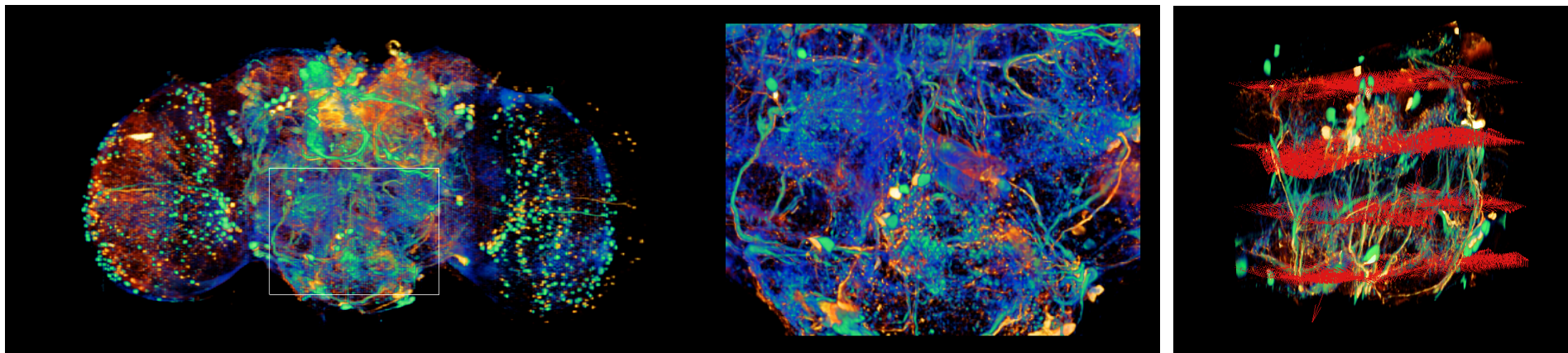
3D example

- Applications in Biological Imaging - Fly Brain(3D)

Overlay of Fluorescent Images Before and After motion.

Blue: Before motion, Orange: After motion.

Result of 3D Image Velocity Field Calculation



Source image:
Before motion

Register image 1

Register image 2

Target image:
After motion



Conclusion

1. Based on continuum mechanics, this research develops a novel finite element method for computational mechanics and conducts scientific experimental research on related microfluidic systems.
2. It is possible to derive the uncertain response of a Stokes flow in Euler space for any degree of freedom under random external conditions. Therefore, it is possible to predict and control the service performance and quality of mechanical system design effectively and efficiently.
3. By performing actual measurements, it is possible to analyze the measurement error of any degree of freedom of a Stokes flow in Euler space. This allows the measured data of the fluid field to comply with the fluid governing equations and eliminates concerns regarding distorted signals due to noise reduction.



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